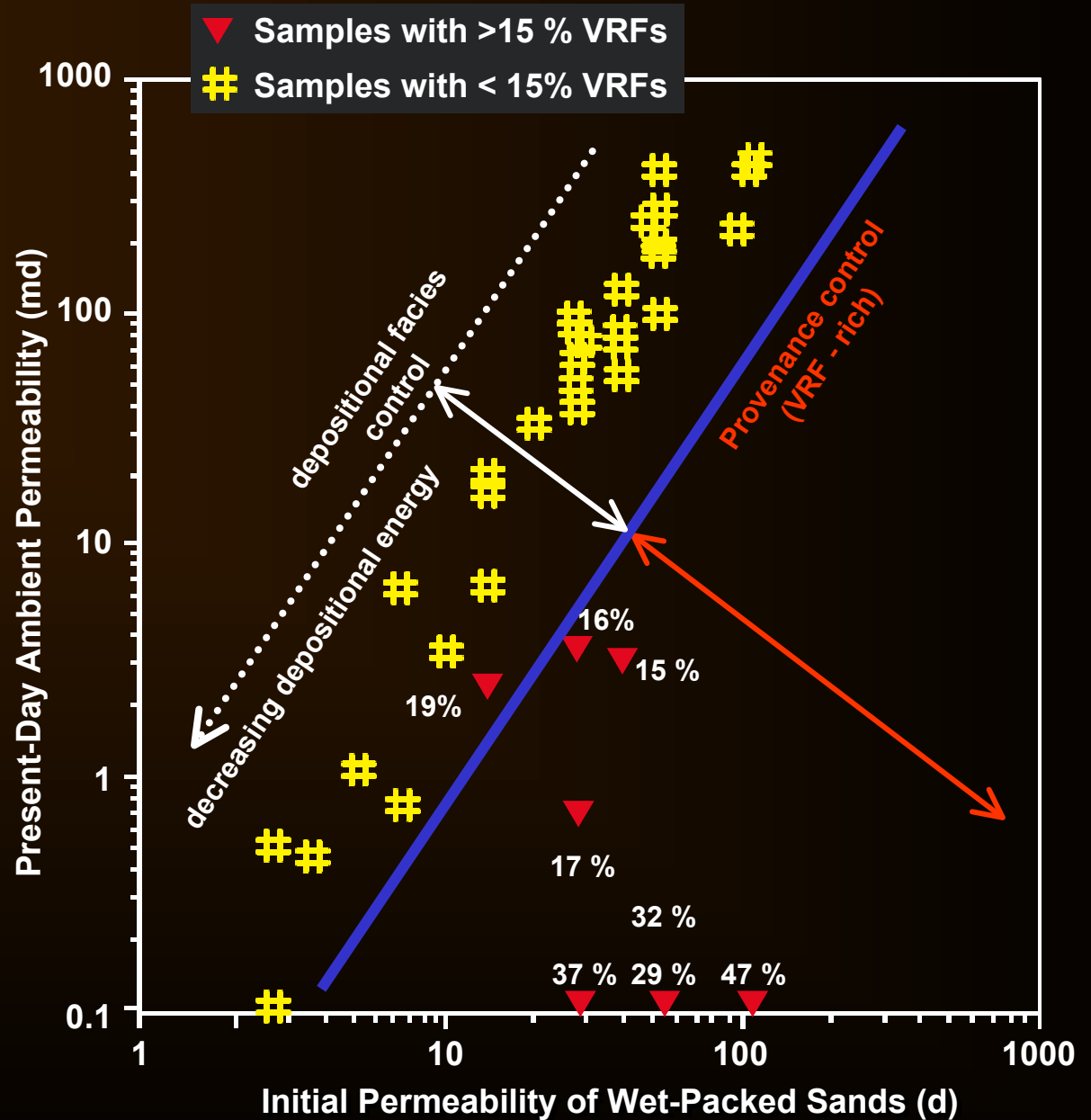


# Predrill Assessment of p&p in Frontier and Mature Areas

by  
S. Bloch

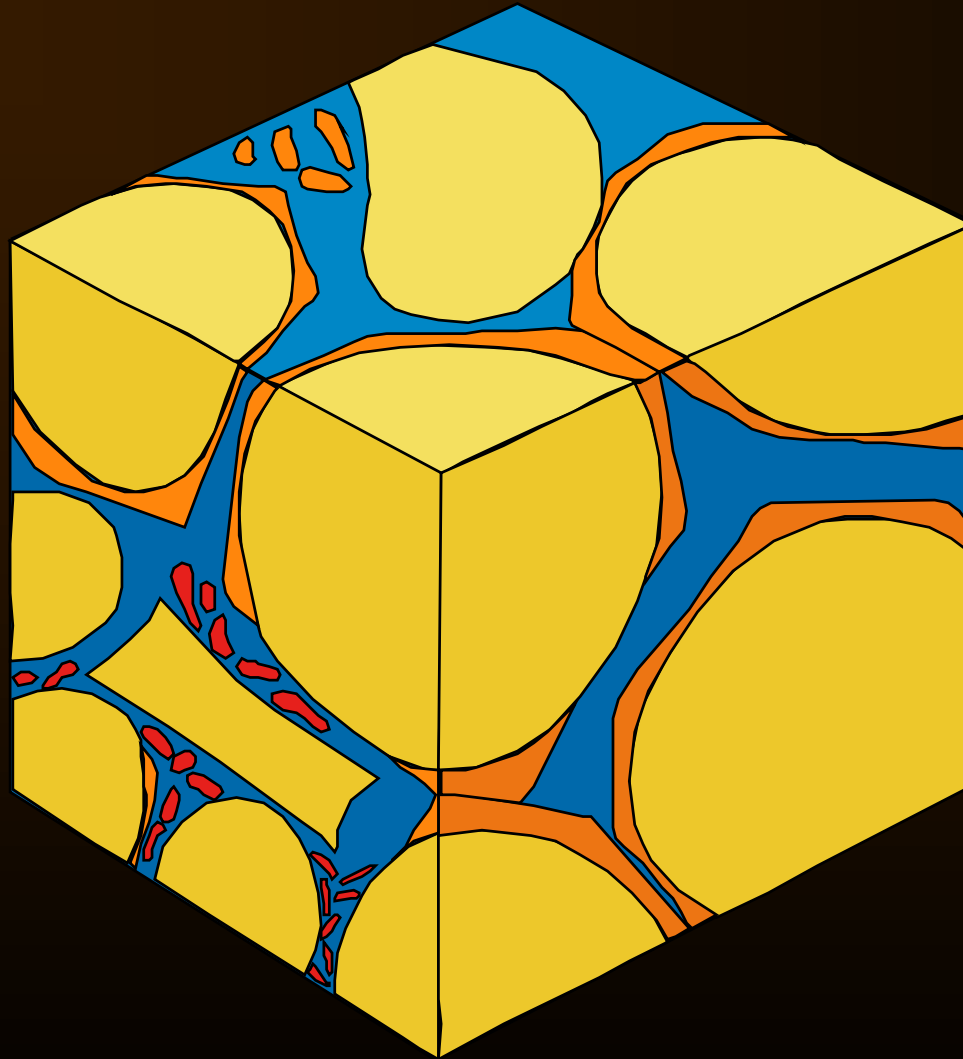


Graphics: P. M. Kay

**© 2001 The American Association of  
Petroleum Geologists and Salmon Bloch**

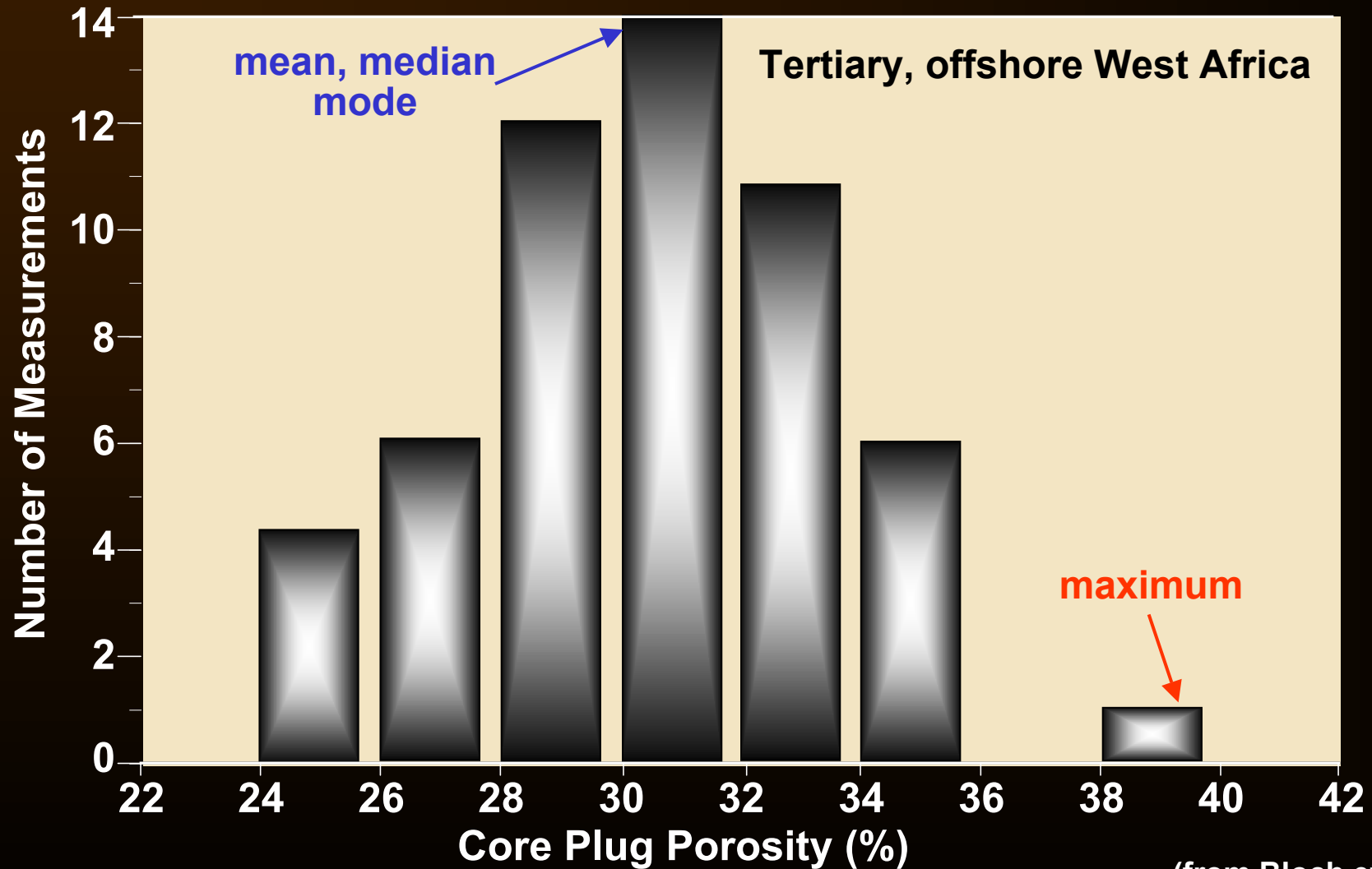
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# Volumetric Components of Sandstones



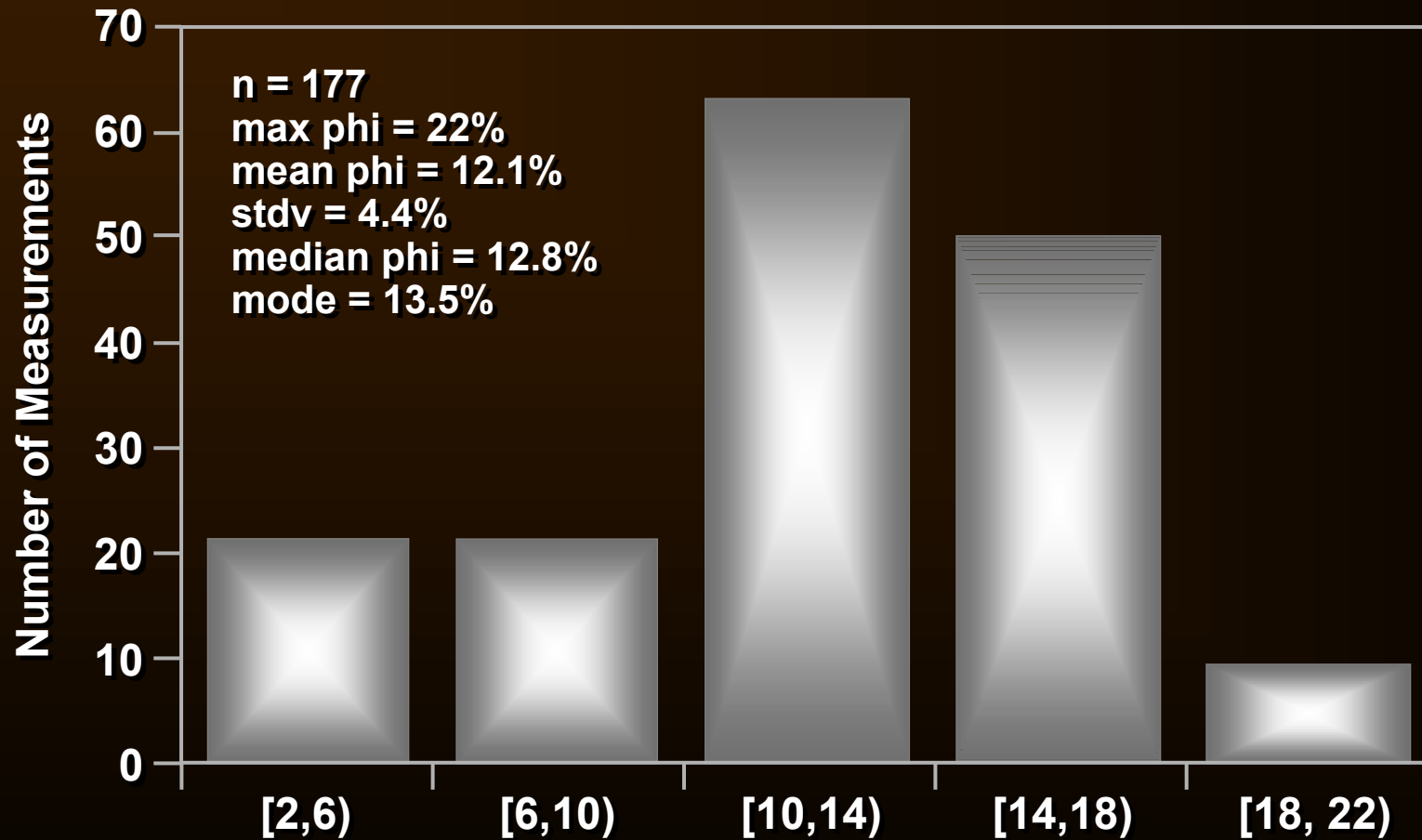
- detrital grains
- matrix
- cement
- pores

# Normal Distribution of Porosity in a Sandstone with a Moderate Diagenetic Imprint

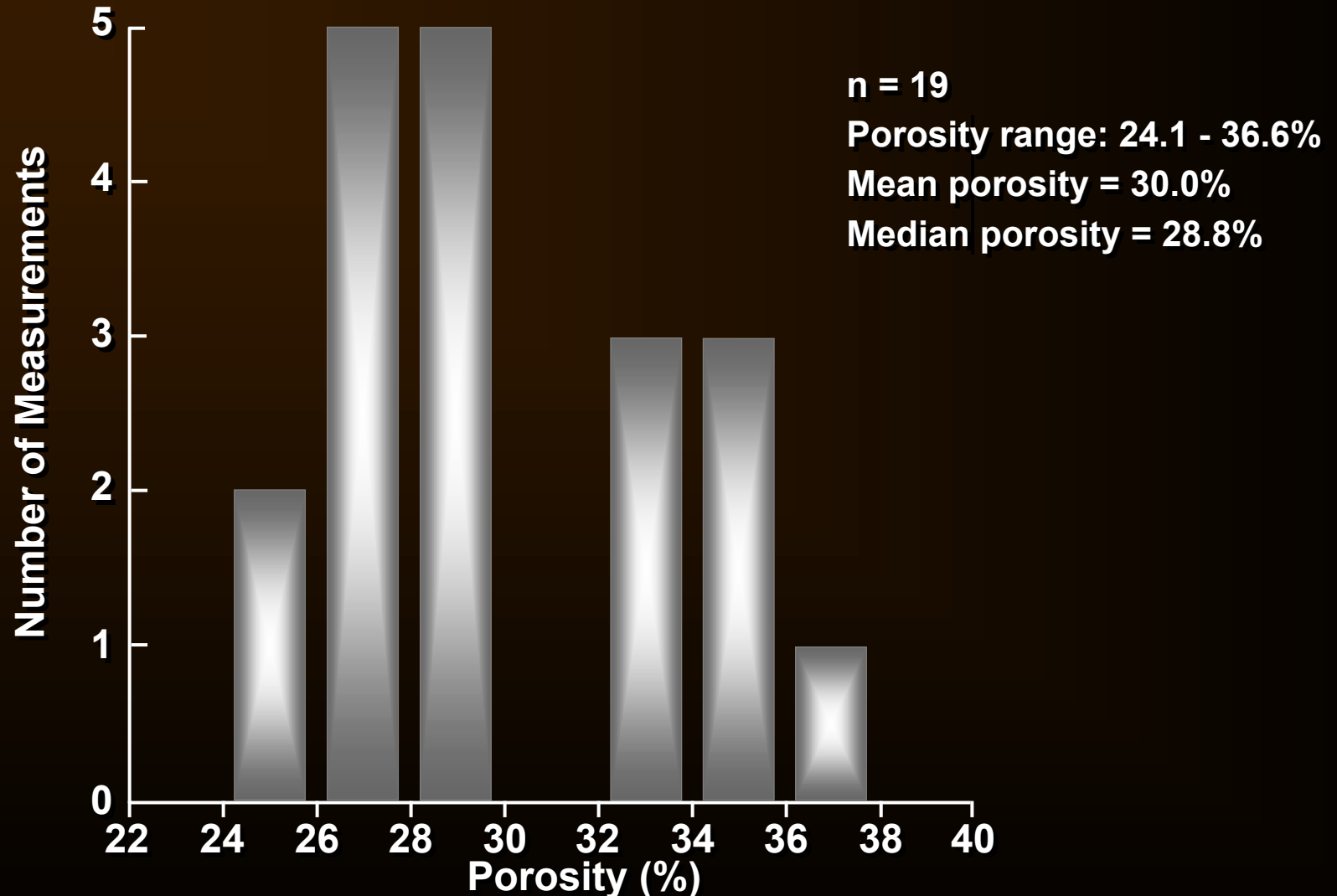


(from Bloch et al., 2002)

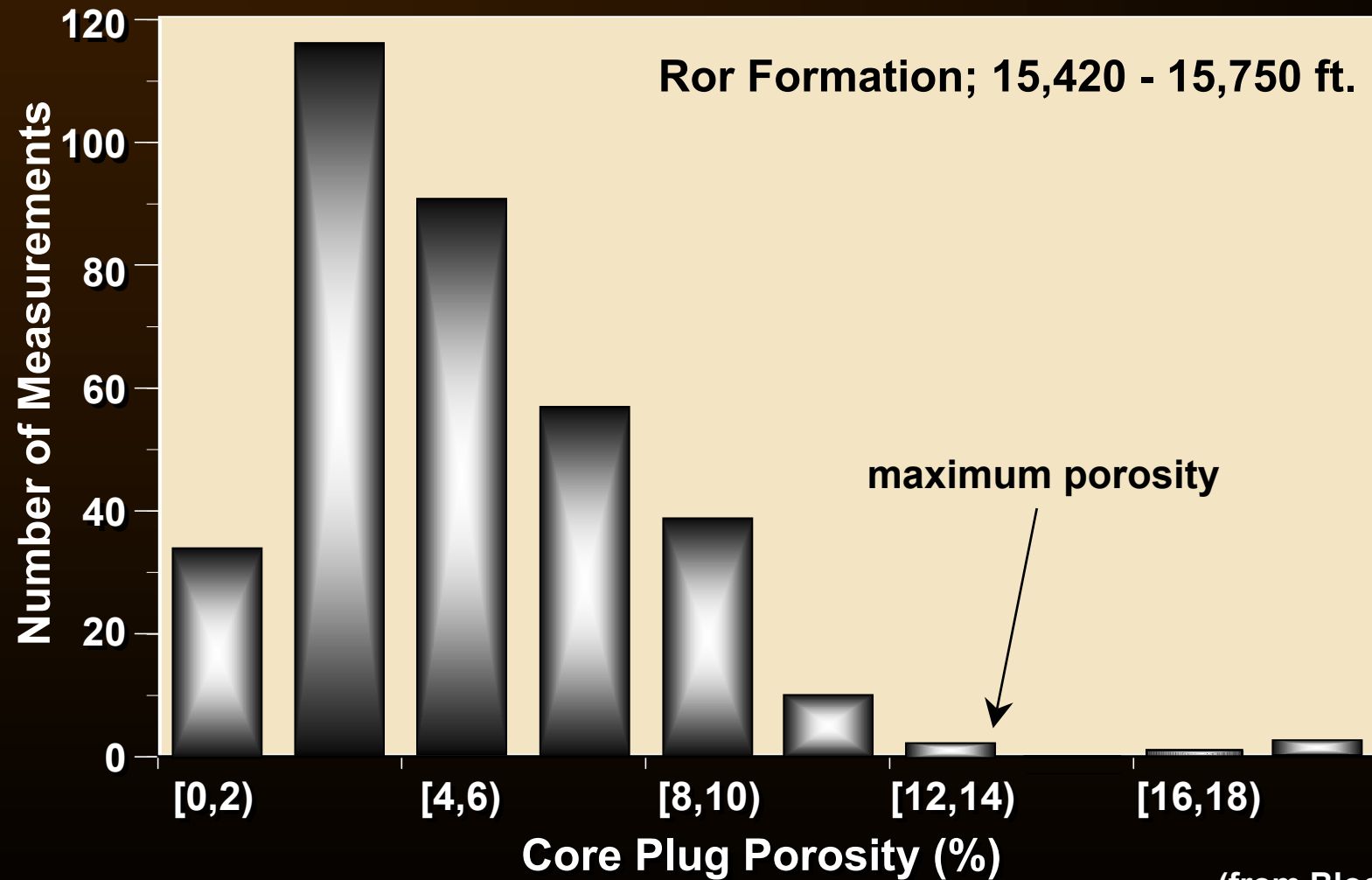
# Porosity Distribution in Sampled Intervals of an Oligocene Sandstone, East Asia



# Porosity Distribution in an Inadequately Sampled Sand Population



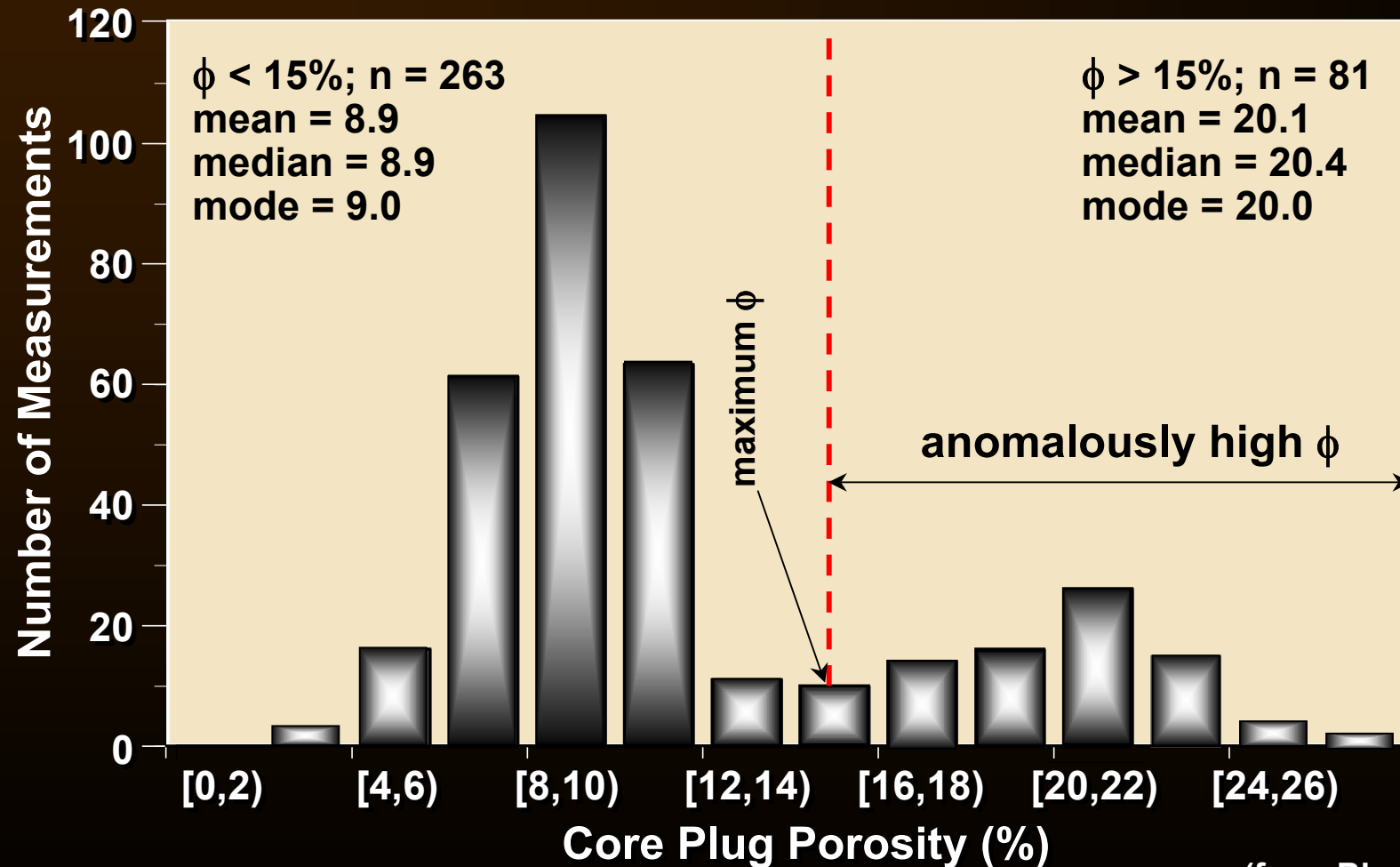
# Lognormal Distribution of Porosity in Heavily Cemented Sandstones



(from Bloch et al., 2002)

# Bimodal Distribution of Porosity in Chlorite-Coated Sandstones

Ile Formation; 15,100 - 15,420 ft.



(from Bloch et al., 2002)



# Applications of Porosity & Permeability Prediction

## ➤ Exploration

- pre-drill evaluation of resources in potential reservoirs

## ➤ Production

- pore volume, hydrocarbon pore volume, recoverable reserves, production rates, well spacing, fluid injection, etc.

## ➤ Reservoir Simulation

- “soft” input data

## ➤ Basin Modeling

- hydrocarbon migration
- distribution of hydrocarbon saturation
- thermal conductivity

## ➤ Interpretation of Seismically Derived Attributes

- porosity, lithology, fluid saturation → acoustic impedance

# Adequacies of Essential Geologic Controls of Oil & Gas for Plays/Prospects

PLAY \_\_\_\_\_ PROSPECT \_\_\_\_\_

a. \_\_\_\_\_ TRAP - SEAL - TIMING

Closure Volume

Seal

Timing

b. \_\_\_\_\_ RESERVOIR - POROSITY - PERMEABILITY

👉 RESERVOIR FACIES THICKNESS (no nondeposition, facies change, truncation, or faulting; adequate net/gross

👉 POROSITY (primary or secondary, not plugged or cemented)

👉 PERMEABILITY & CONTINUITY

c. \_\_\_\_\_ SOURCE - MATURATION - MIGRATION

Organic Quantity & Quality

Maturation

Migration

d. \_\_\_\_\_ PRESERVATION - HC QUALITY - RECOVERY

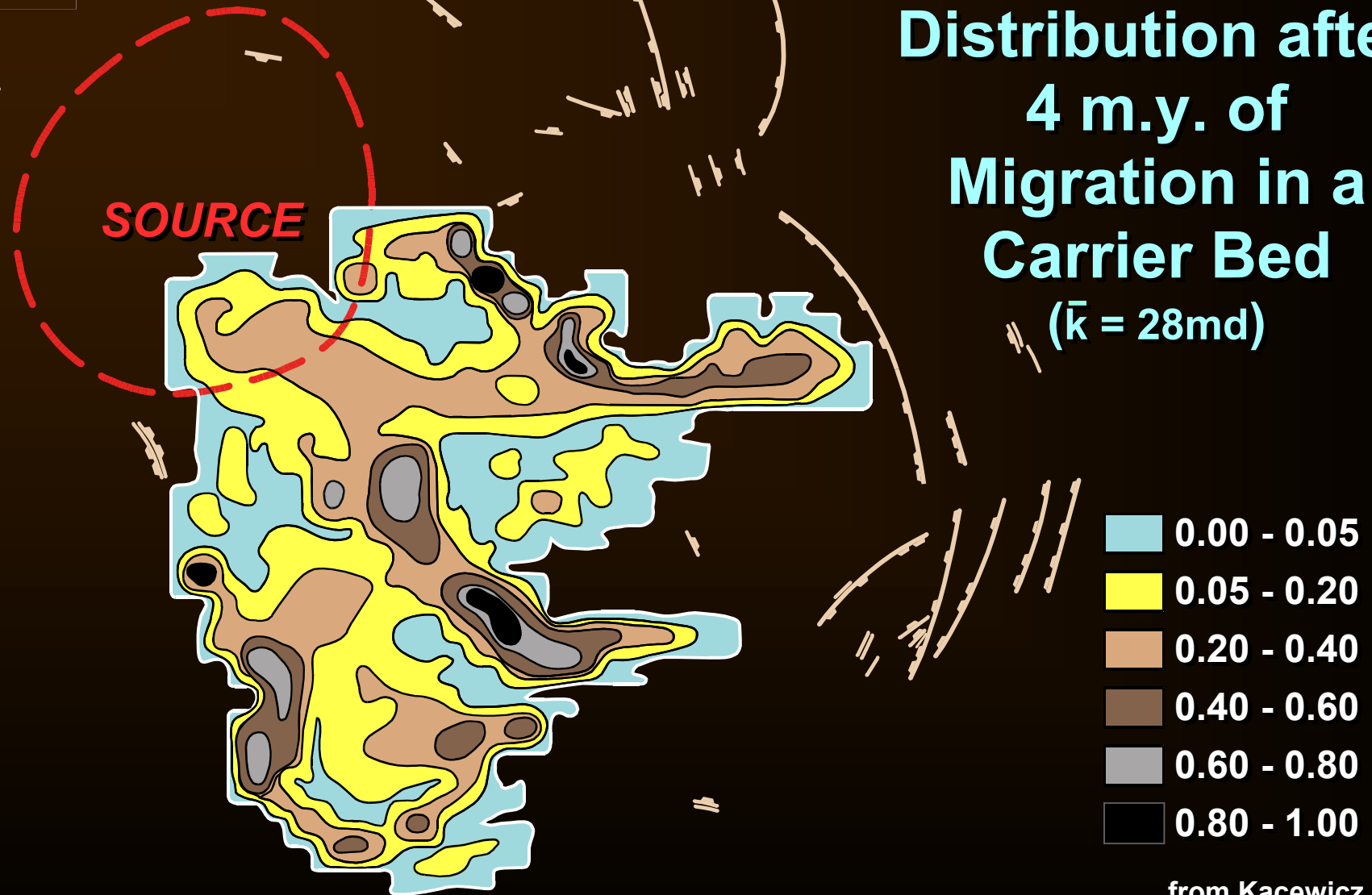
Preservation

Hydrocarbon Quality & Concentration

Recovery

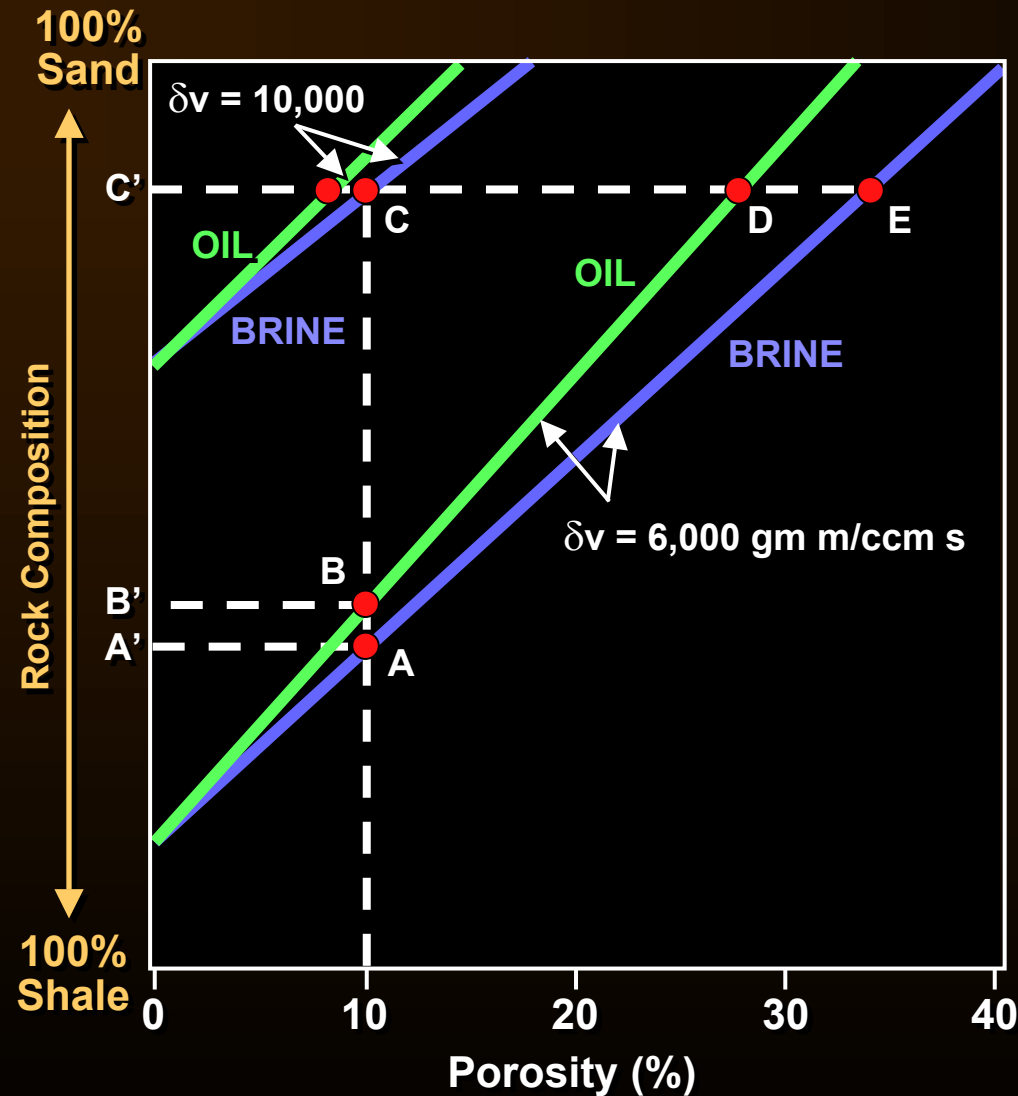
(from White, 1993)

# Oil Saturation Distribution after 4 m.y. of Migration in a Carrier Bed ( $\bar{k} = 28\text{md}$ )



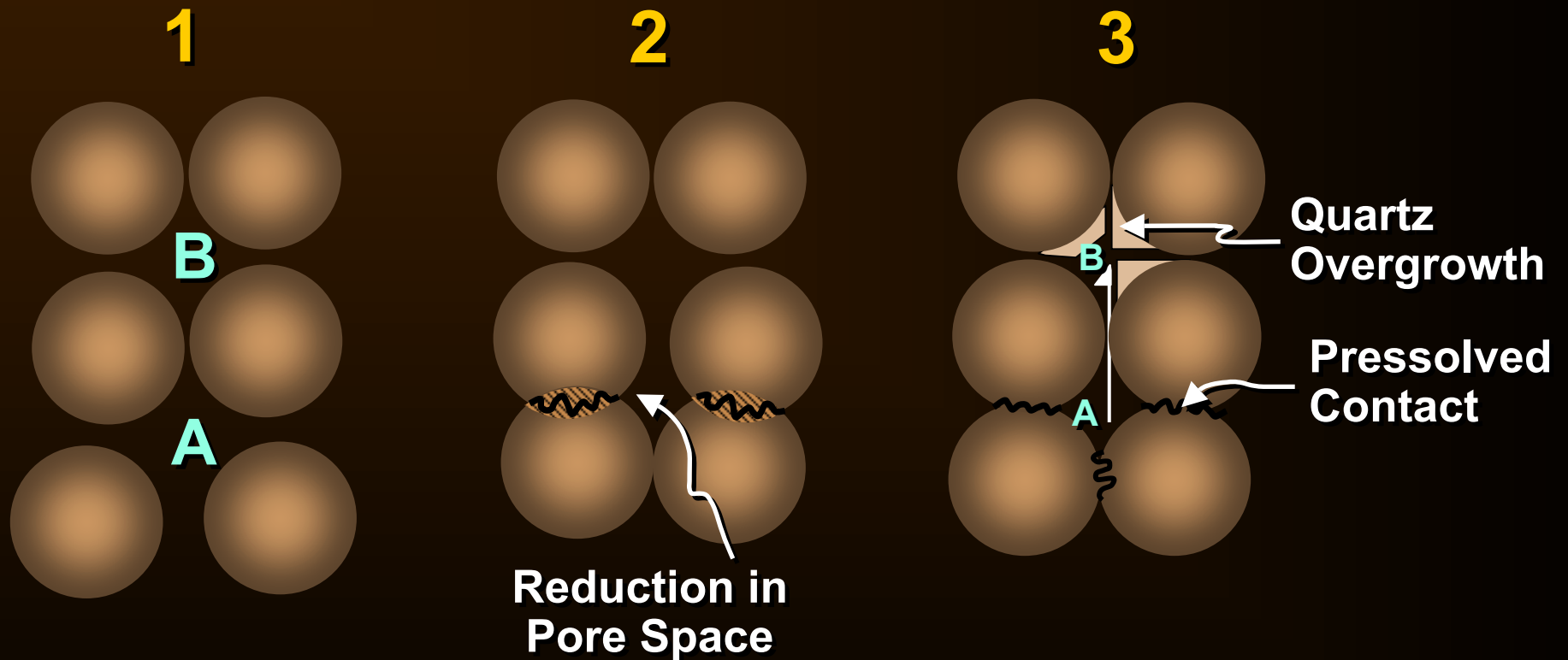
from Kacewicz, 1993

# Reservoir Properties (lithology, porosity, pore fluid) vs Acoustic Impedance



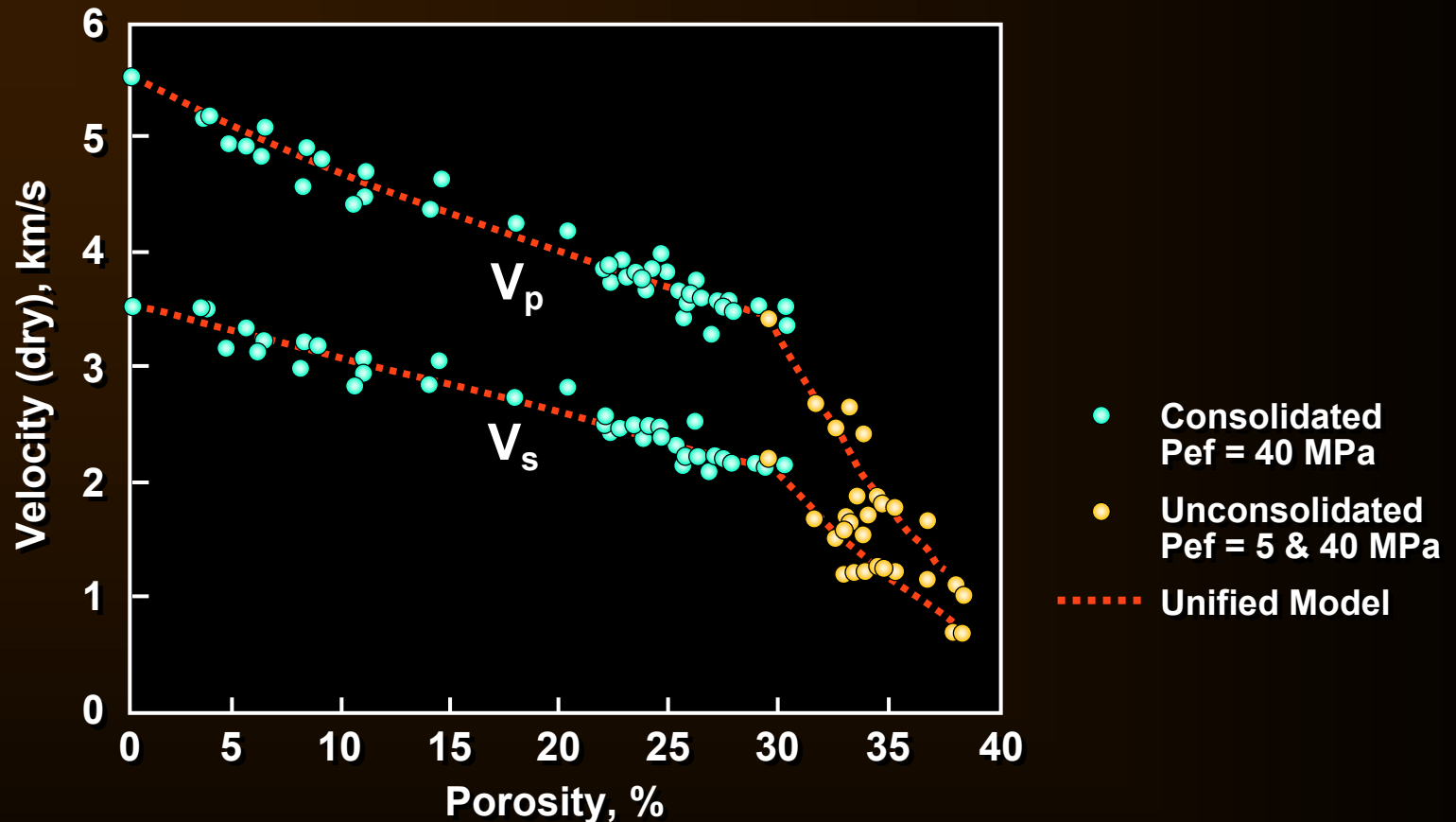
(from Hardage, 1992)

# Silica Cementation by Pressure Solution



(from Sibley and Blatt, 1976)

# Consolidation Porosity vs. $V_p$ and $V_s$



For **moderately well-sorted** sands “consolidation porosity” for clean arenites is 30%, and for arenites 29%. Clean arenites have  $< 2\% V_{\text{clay}}$ , arenites have  $2\% - 12\% V_{\text{clay}}$ . The transition from “unconsolidated” to “consolidated” sands (at 30% to 29% porosity) is expressed by pronounced deflections in dry frame P- and S-wave velocities. Fluid substitution modeling indicates a negligible fluid effect on velocity below the consolidation porosity of 29% to 30%.

(Vernik, 1998)

**Sandstone  
Reservoir Quality**

```
graph BT; P[Provenance] --> SRQ[Sandstone Reservoir Quality]; DE[Depositional Environment] --> SRQ; PDH[Post-depositional History] --> SRQ; P --> DMC[Detrital Mineral Composition]; DE --> DMC; DE --> T[Texture]; DMC --> SRQ; T --> SRQ;
```

**Provenance**

**Depositional  
Environment**

**Post-depositional  
History**

**Detrital  
Mineral  
Composition**

**Texture**

# **Requirements for Adequate Predictions**

- 1. High predictive accuracy should be achieved from a limited number of geological input parameters**
- 2. Input parameters should be simple enough to be estimated from available geological information with reasonable confidence**
- 3. Prediction should be based on multiple techniques**



# Porosity of Artificially Mixed Sand

SIZE →	COARSE		MEDIUM		FINE		VERY FINE	
↓ SORTING	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER
EXTREMELY WELL SORTED	43.1	42.8	41.7	41.3	41.3	43.5	42.3	43.0
VERY WELL SORTED	40.8	41.5	40.2	40.2	39.8	40.8	41.2	41.8
WELL SORTED	38.0	38.4	38.1	38.8	39.1	39.7	40.2	39.8
MODERATELY SORTED	32.4	33.3	34.2	34.9	33.9	34.3	35.6	33.1
POORLY SORTED	27.1	29.8	31.5	31.3	30.4	31.0	30.5	34.2
VERY POORLY SORTED	28.6	25.2	25.8	23.4	28.5	29.0	30.1	32.6

(from Beard and Weyl, 1973)

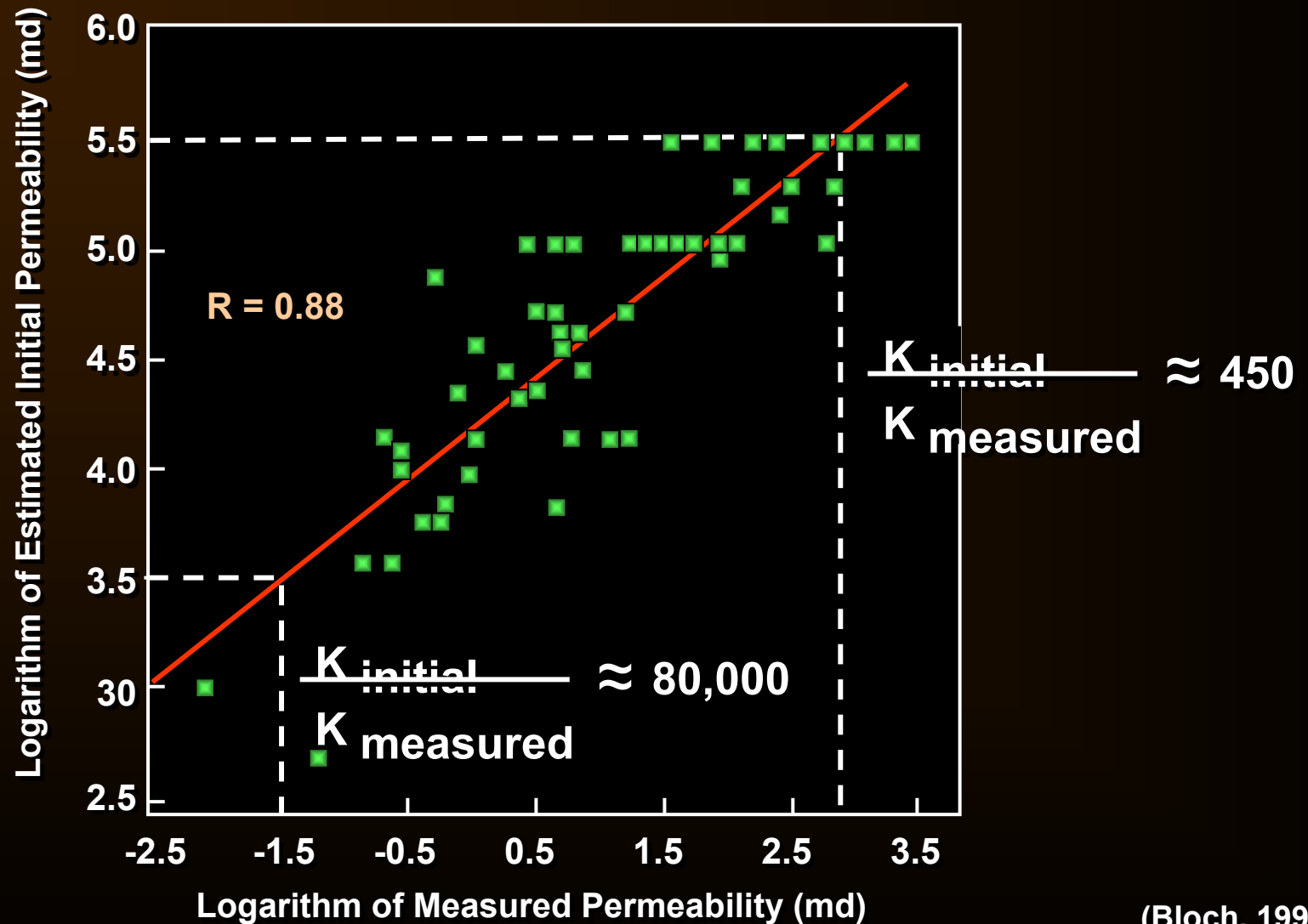
# Average Permeability (Darcys) of Artificially Mixed, Wet-Packed Sand

SIZE →	COARSE		MEDIUM		FINE		VERY FINE	
↓ SORTING	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER
EXTREMELY WELL SORTED	475	238	119	59	30	15	7.4	3.7
VERY WELL SORTED	458	239	115	57	29	14	7.2	3.6
WELL SORTED	302	151	76	38	19	9.4	4.7	2.4
MODERATELY SORTED	110	55	28	14	7.0	3.5	2.1*	1.1*
POORLY SORTED	45	23	12	6.0	3.7*	1.9*	0.93*	0.46*
VERY POORLY SORTED	14	7.0	3.5	1.7*	0.83*	0.42*	0.21*	0.10*

\* from formula of Krumbein & Monk (1942)

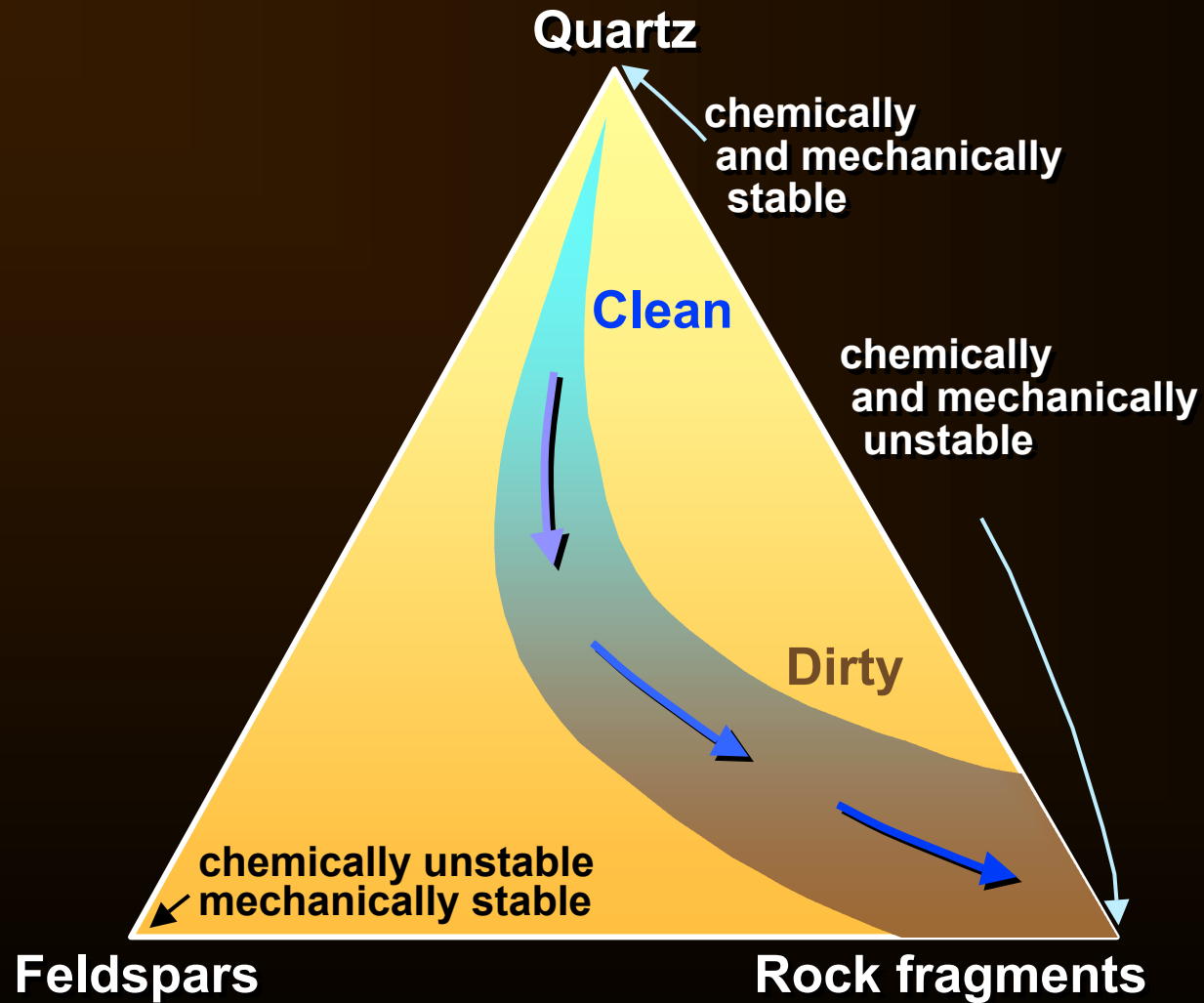
(from Beard and Weyl, 1973)

# Measured Permeability Correlates Well with Estimated Initial Permeability, Yacheng Field



(Bloch, 1991)

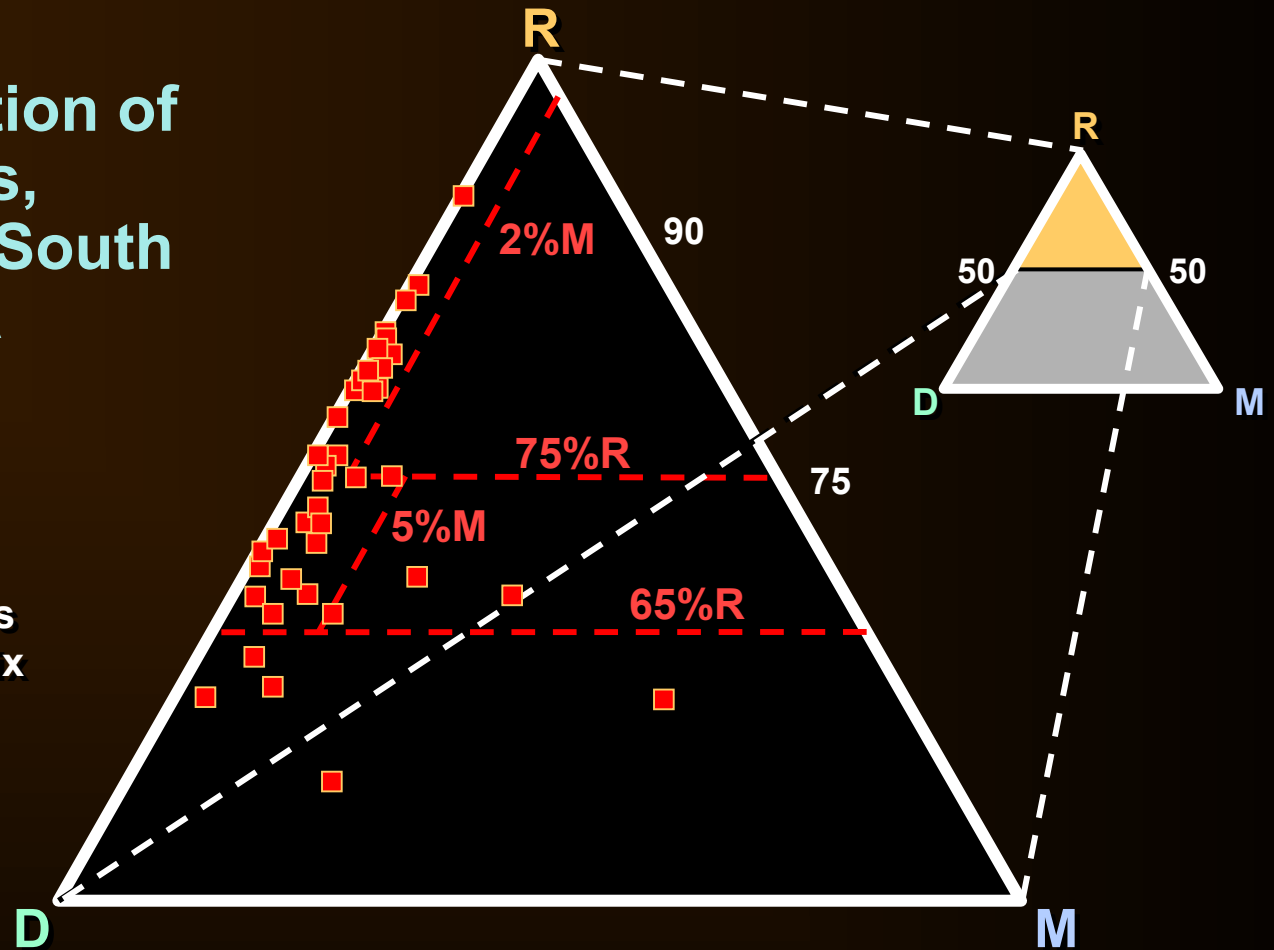
# Compositional Controls on Diagenesis



(from Hayes, 1979)

# RDM Classification of Sandstones, Yacheng Field, South China Sea

**R** = rigid grains  
**D** = ductile grains  
**M** = detrital matrix

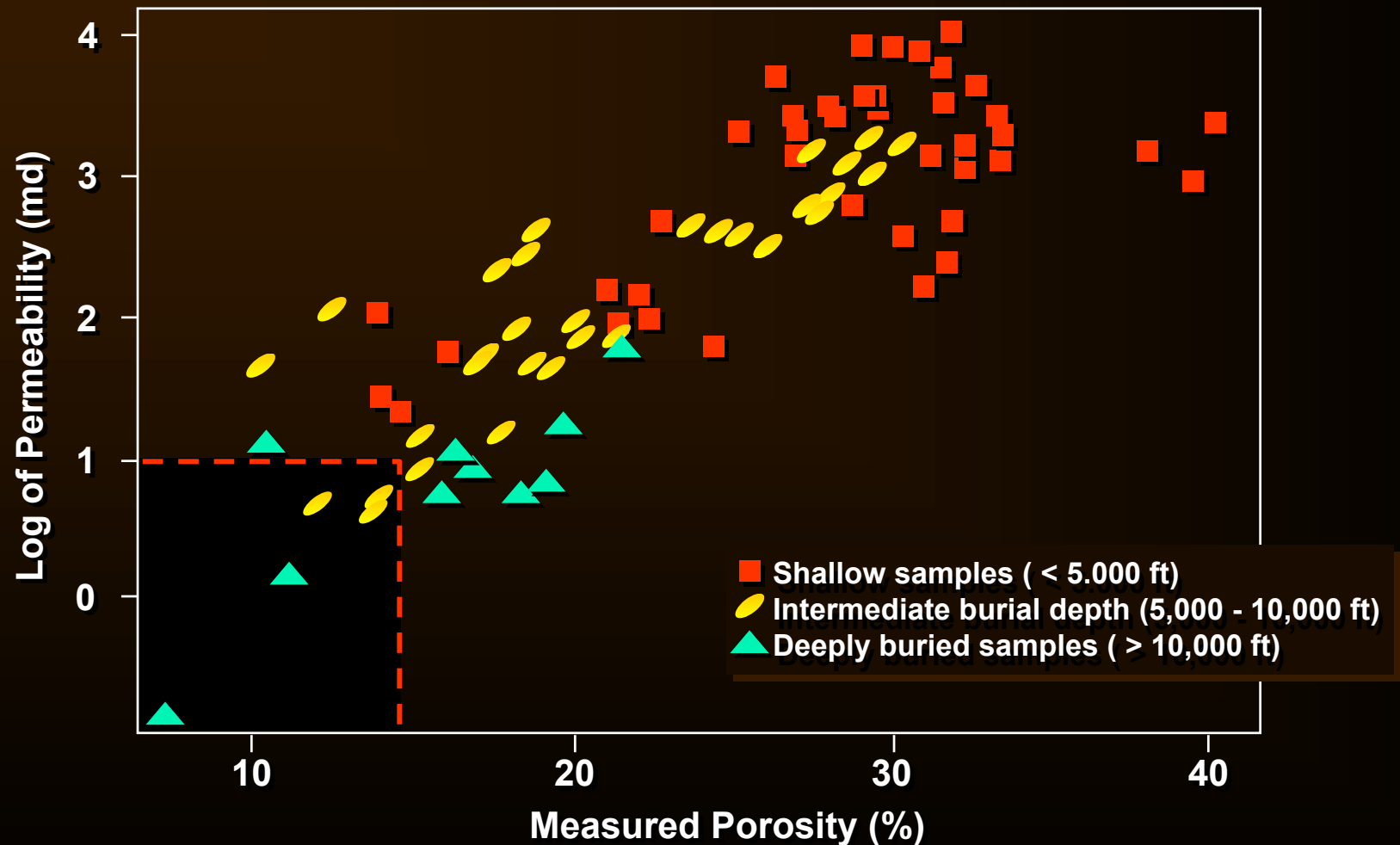


upper medium and coarser grained ss (median diameter > 0.36 mm)

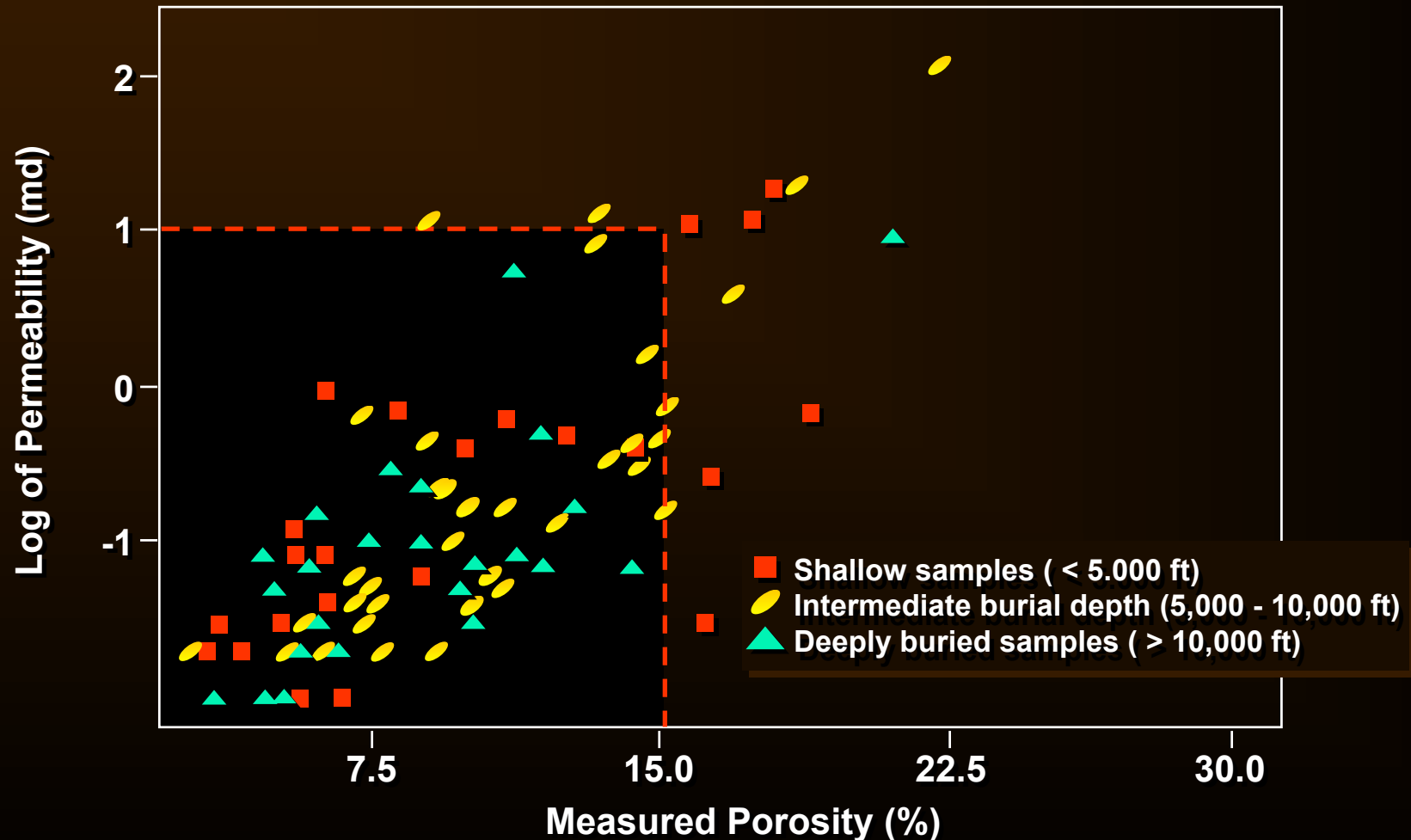
$R > 75\%$ and $M < 2\%$	→	$k > 100$ md	(a few exceptions)
$75\% > R > 65\%$ and $M < 5\%$	→	$k < 100$ md	(a few exceptions)
$R < 65\%$	→	$k < 1$ md	(a few exceptions)

(Bloch, 1991)

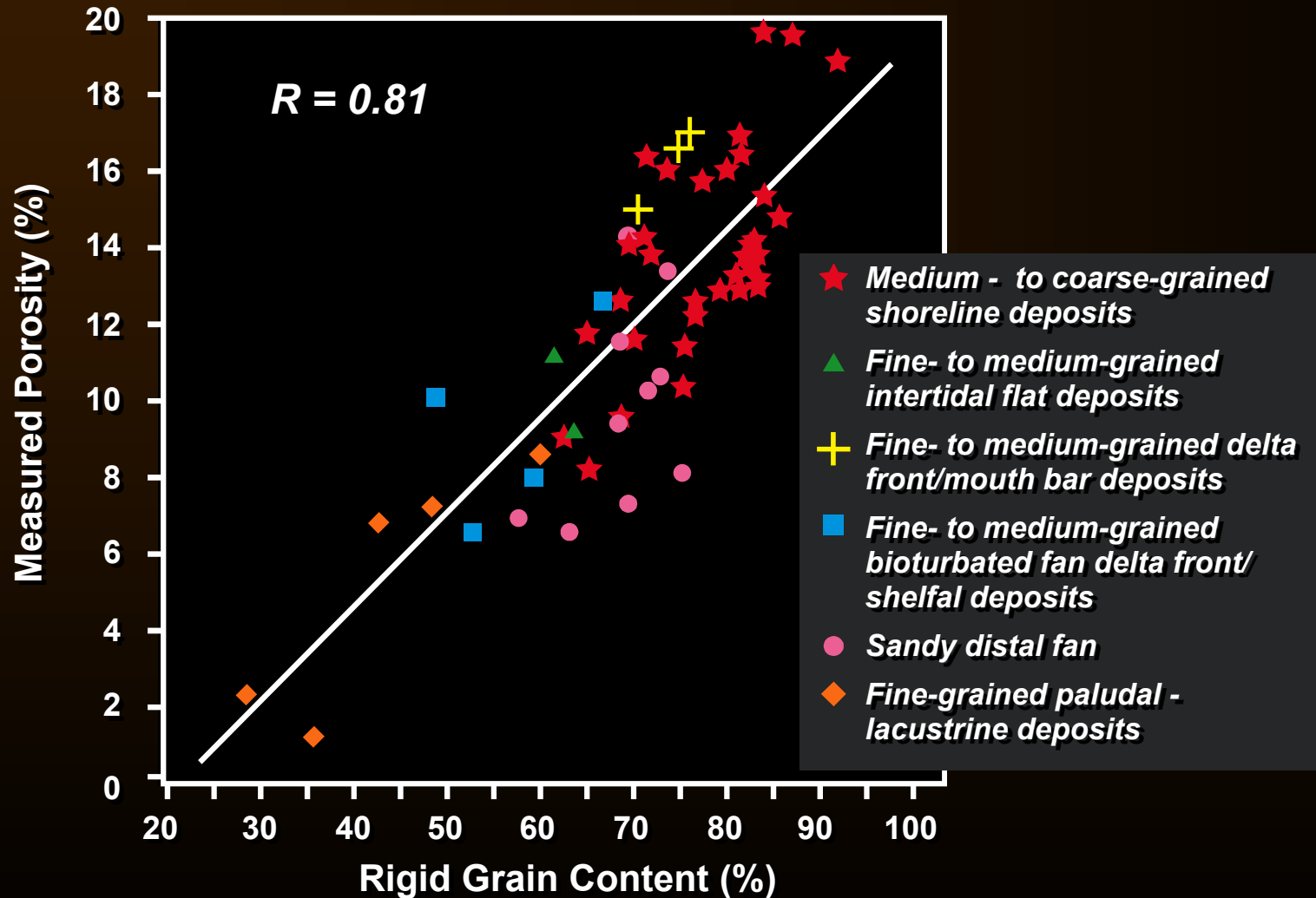
**Weakly-cemented (<10% cement) sandstones with a rigid grain content >85% generally have high porosity and permeability**



**Weakly-cemented (<10% cement) sandstones with a rigid grain content <70% have low porosity and permeability**

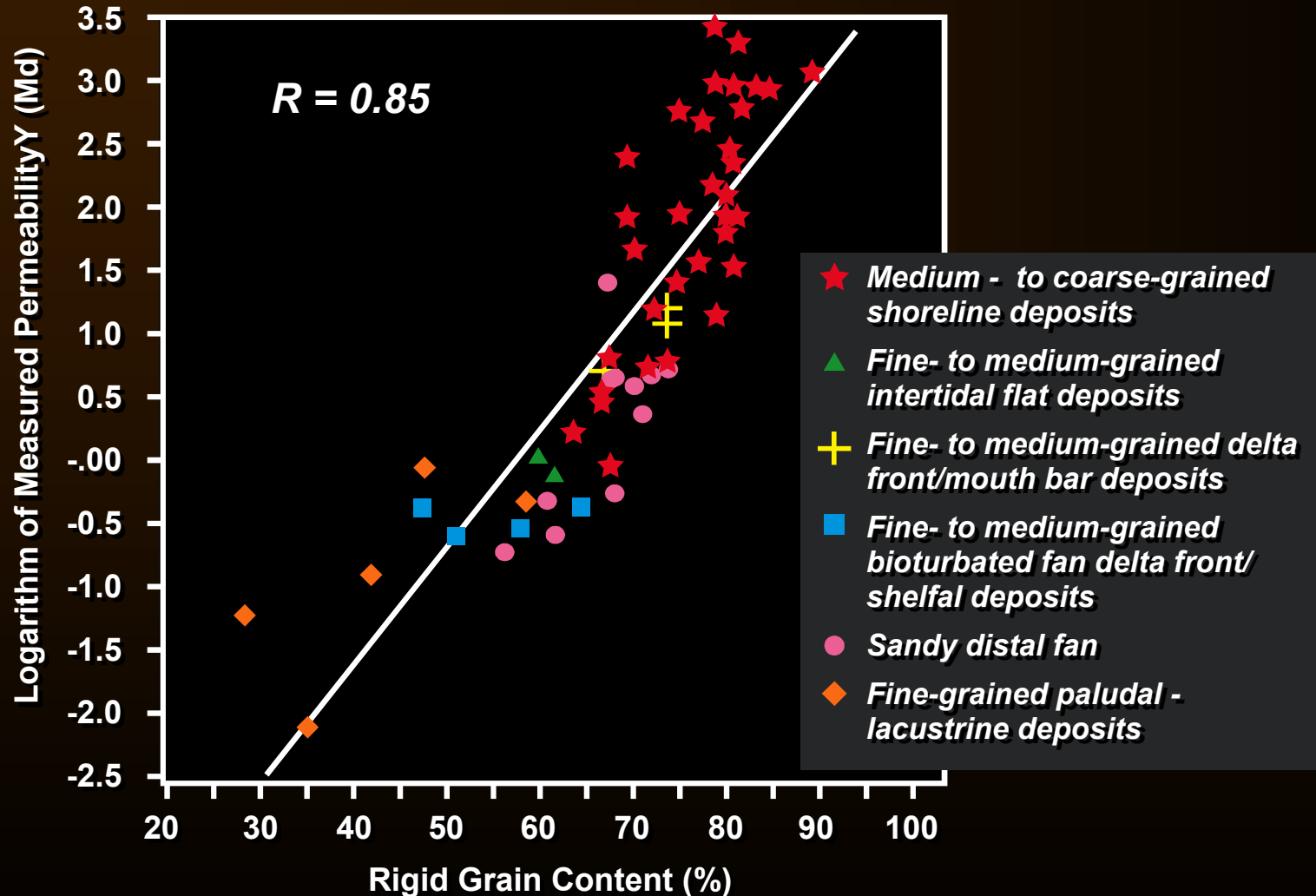


# Measured Porosity Correlates Well with Rigid Grain Content

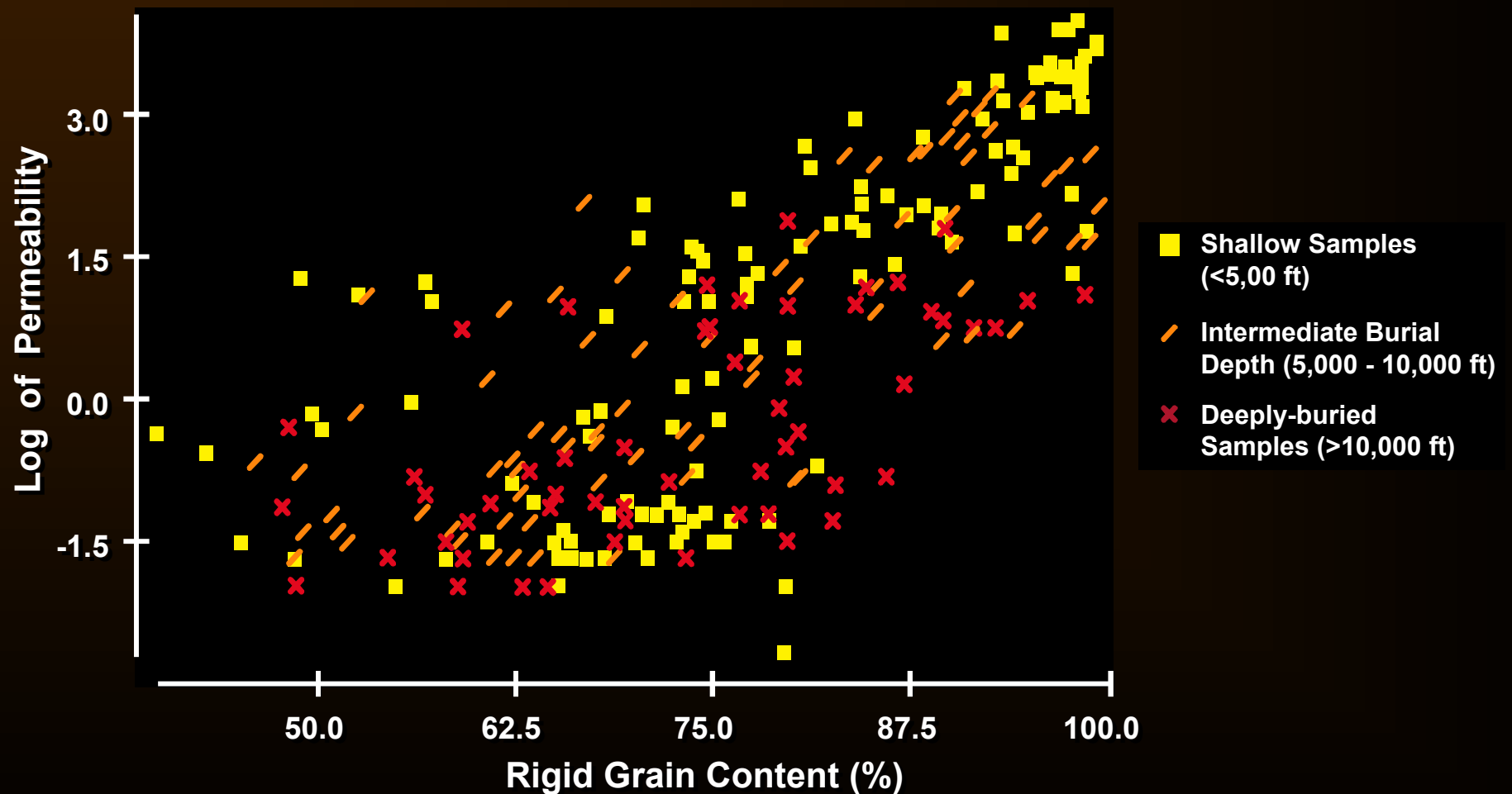




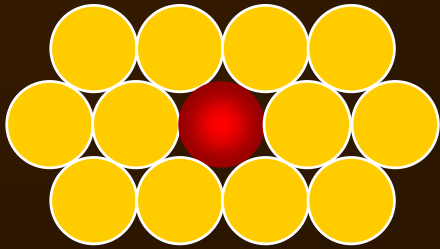
# Measured Permeability Correlates Well with Rigid Grain Content



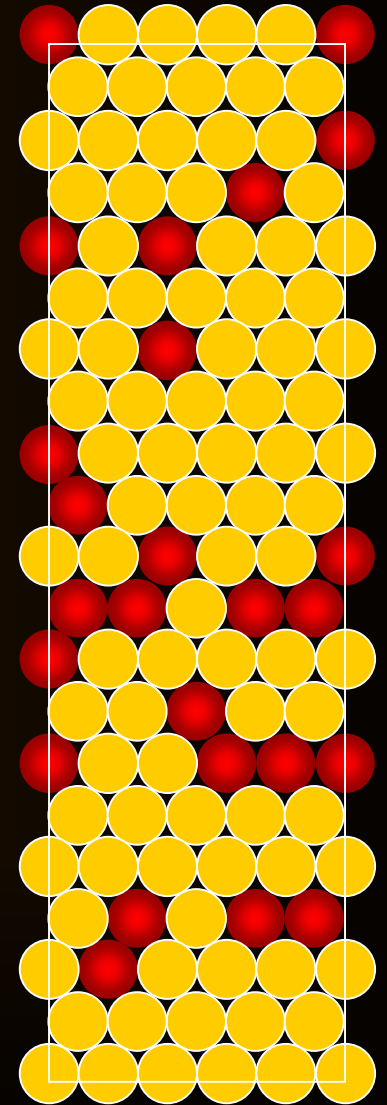
# Permeability in weakly-cemented samples (<10% cement) correlates well with detrital composition (rigid grain content)



# Compaction of Ductile Grains is a Function of Sorting

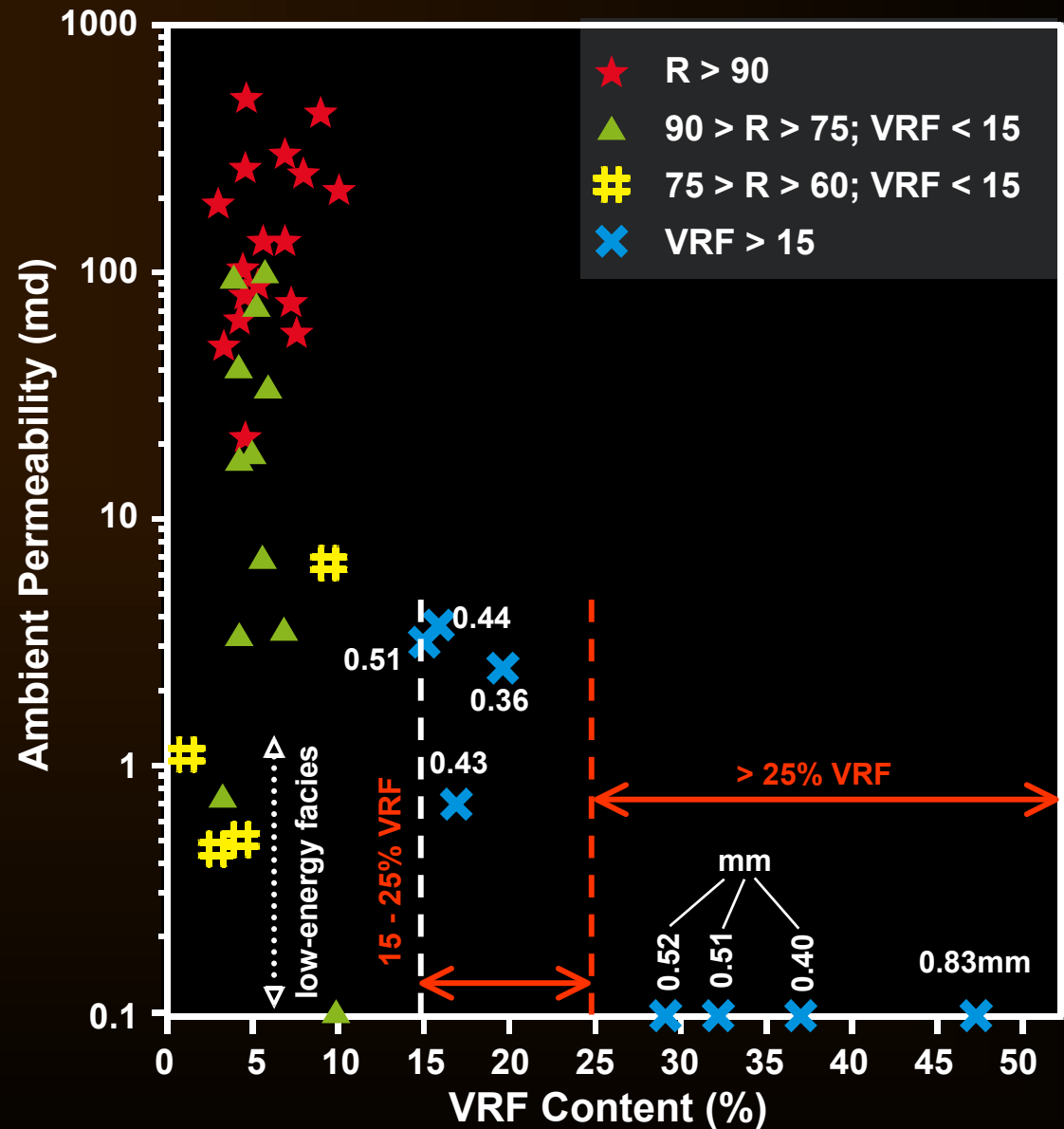


- ▶ A ductile grain (brown) can be protected from compaction by bridging of rigid grains
- ▶ Example of random distribution of ductile grains in a sandstone
- ▶ Although the abundance of ductile grains is 20%, only 15% are in deformable positions

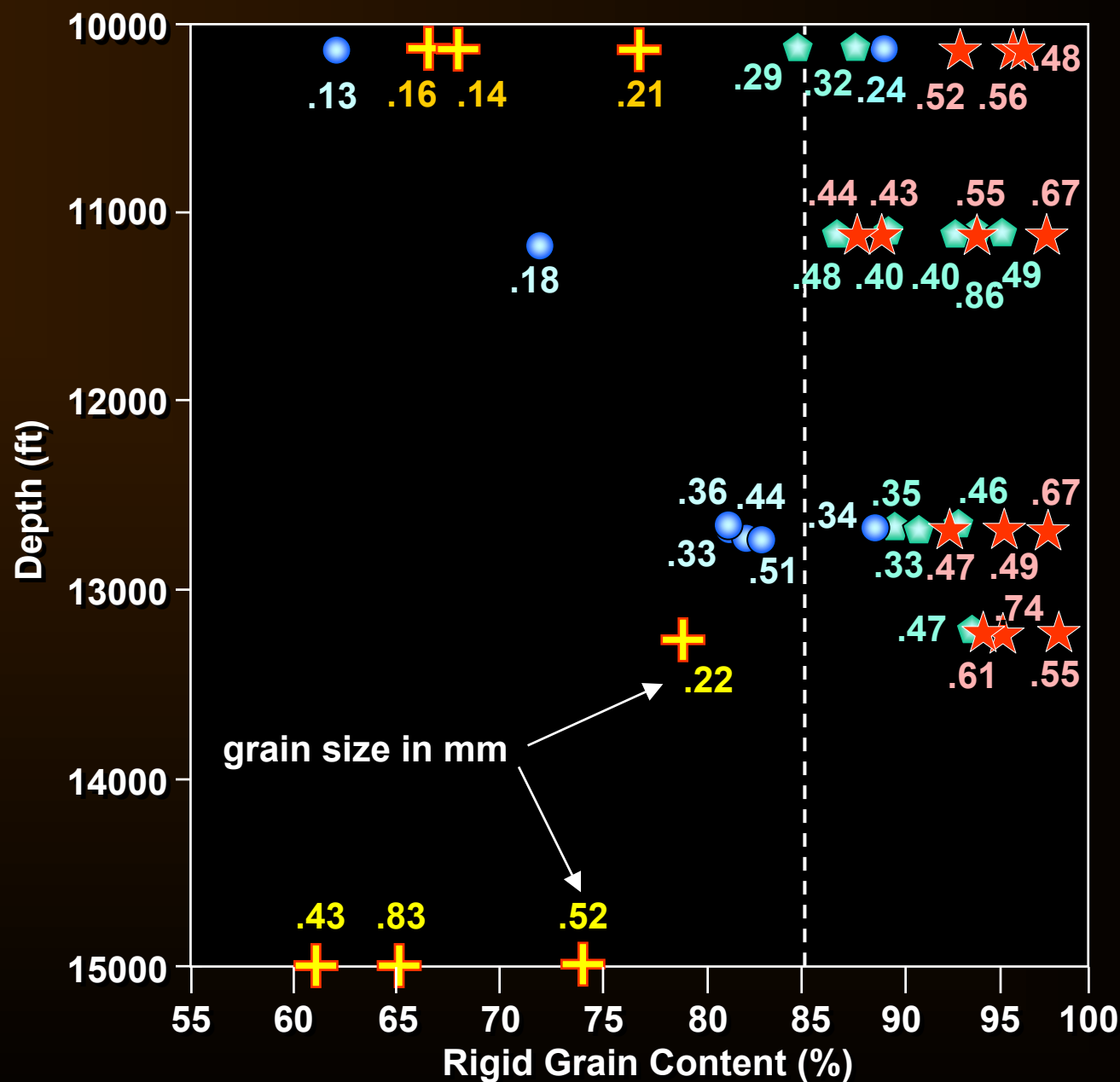


(from Franks, 1981; unpub.)

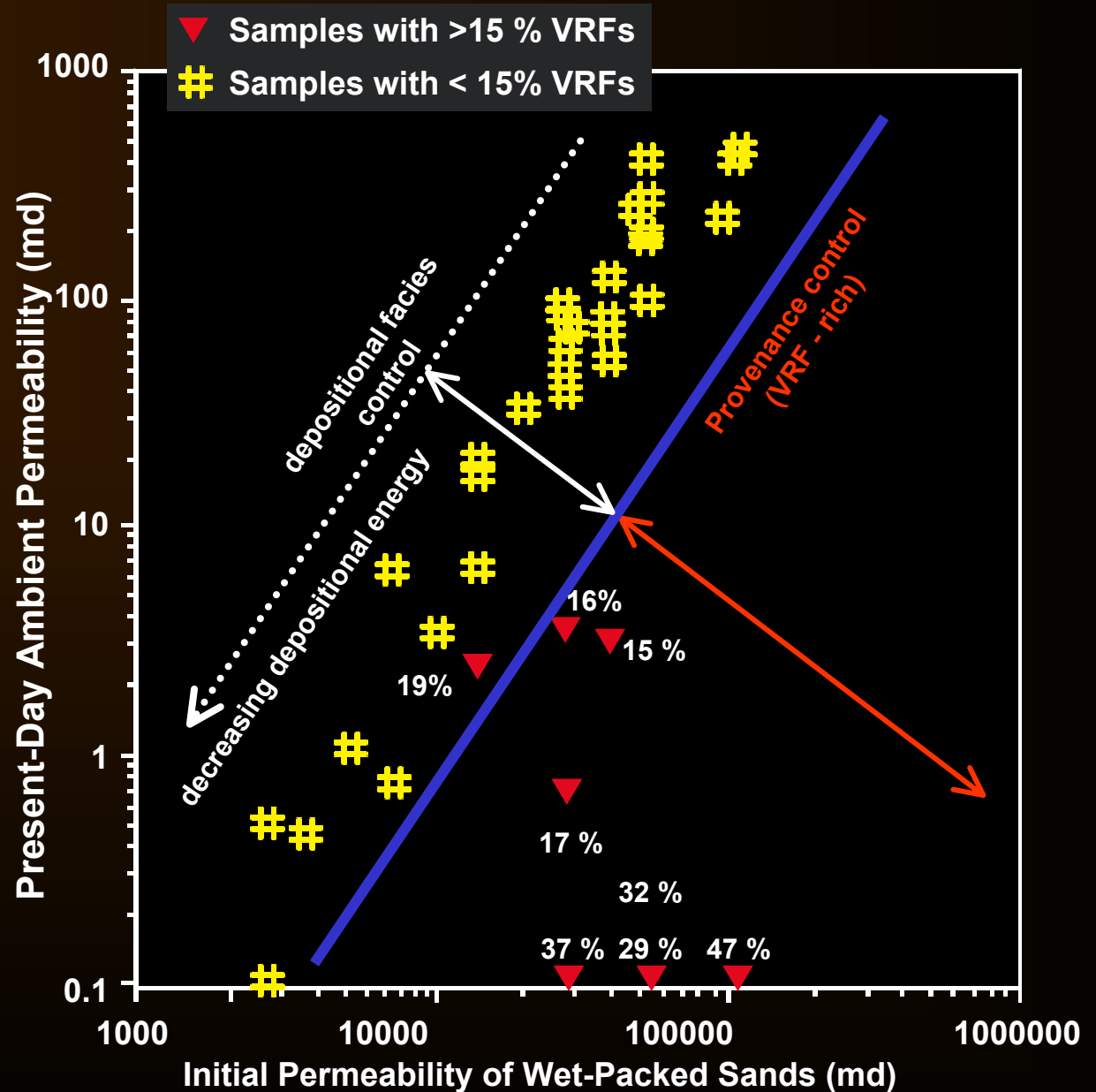
In sandstones with  
VRFs > 25%,  
permeability is very low  
regardless  
of grain size, at  
depths > 10,000 ft



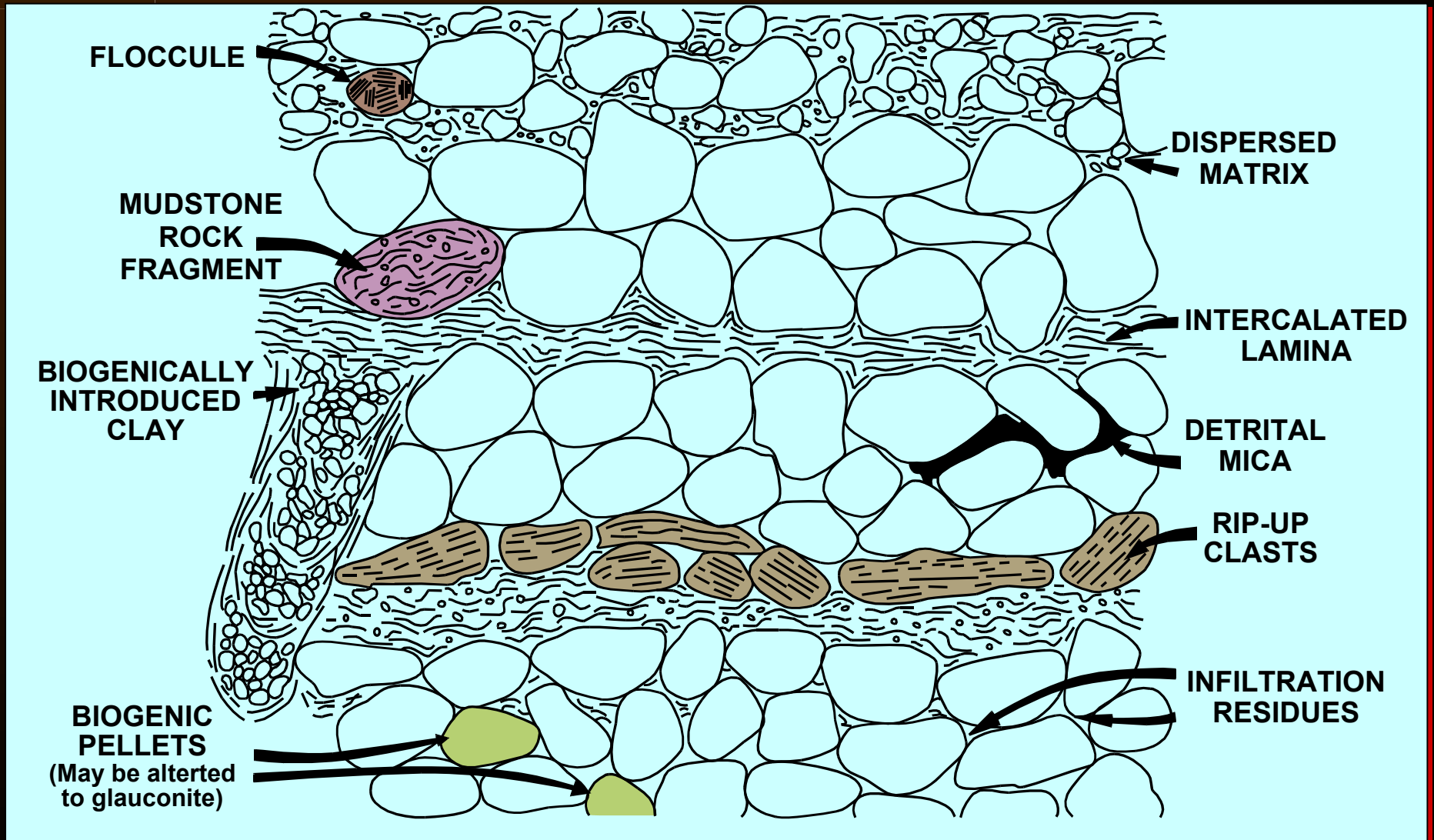
Permeability is not a function of depth in the 10,000 - 13,500 ft interval (in weakly cemented sands;  $\Delta T / \Delta Z \approx 20^{\circ}\text{C/km}$ )



There is an excellent correlation between initial and present-day permeability in weakly cemented sandstones (<10% cement), except for VRF-rich samples

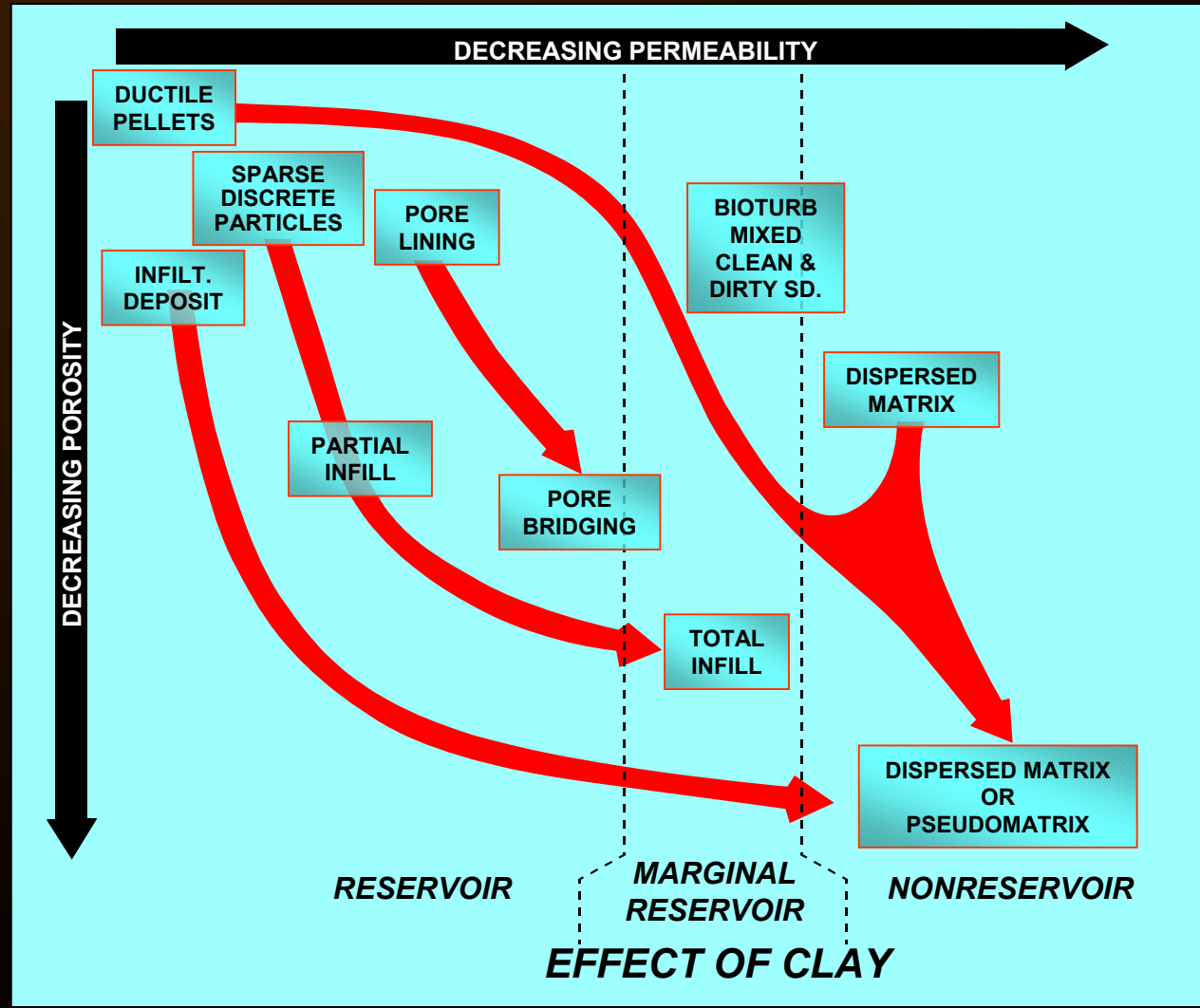


# Modes of Occurrence of Allogenic Clay in Sandstones



(from Wilson and Pittman, 1977)

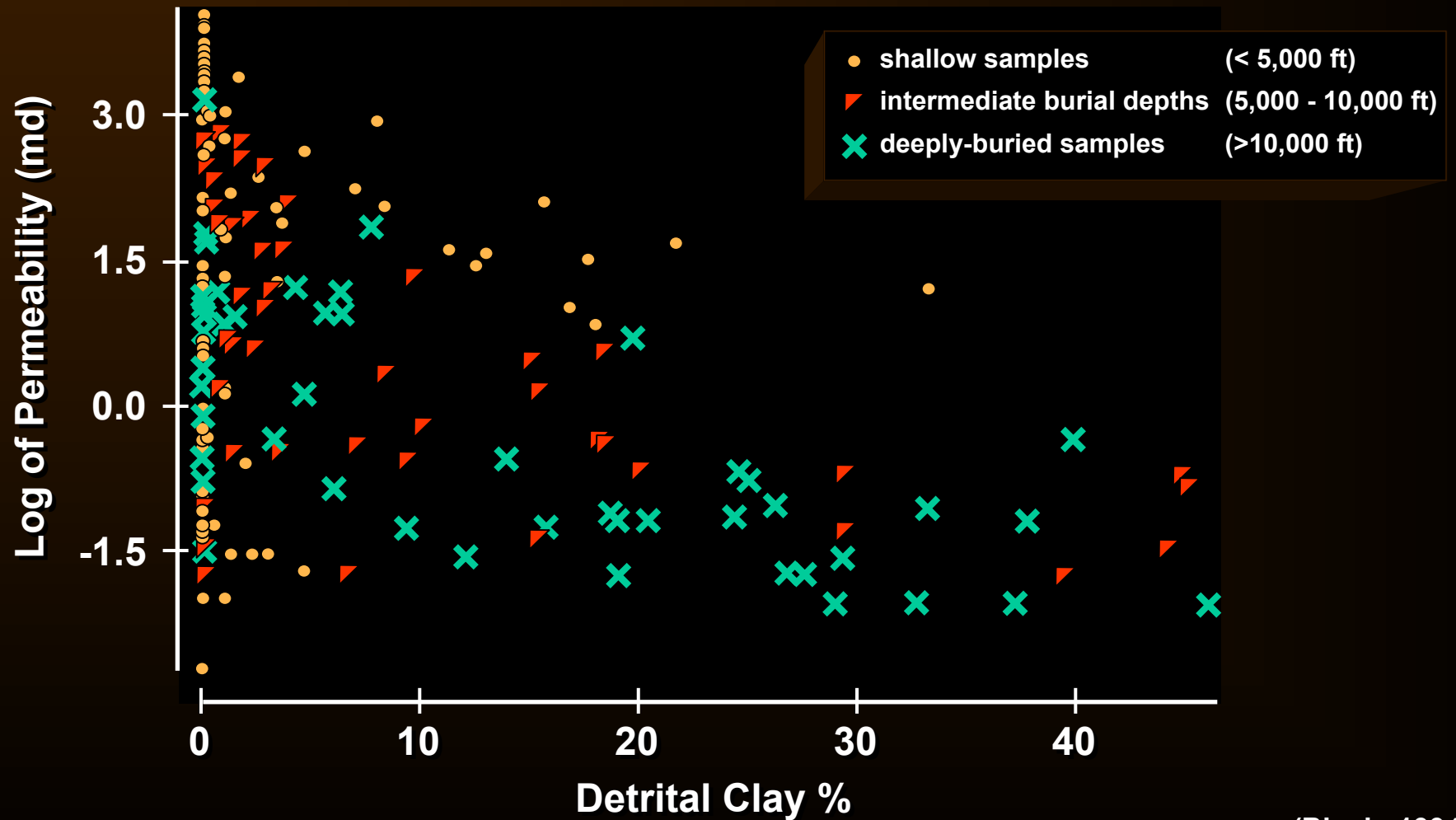
# Porosity and Permeability in Sandstone are Affected by the Amount and Mode of Occurrence of Clay Minerals, and by the Amount of Compaction



(from Pittman, 1989)

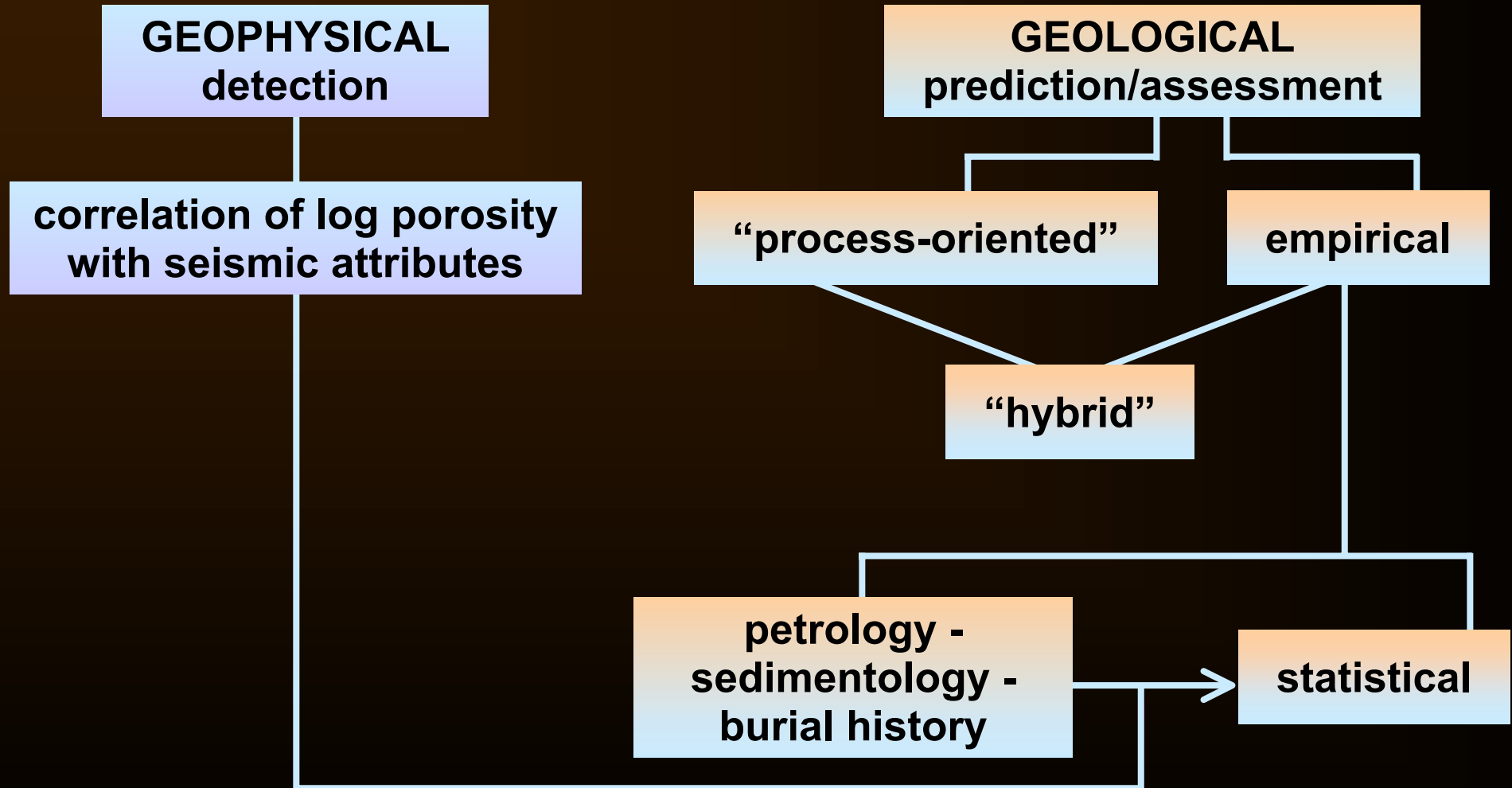


There is no discernible correlation between  $k$  and detrital clay abundance but sandstones with  $>20\%$  of detrital clay generally have low  $k$



(Bloch, 1994)

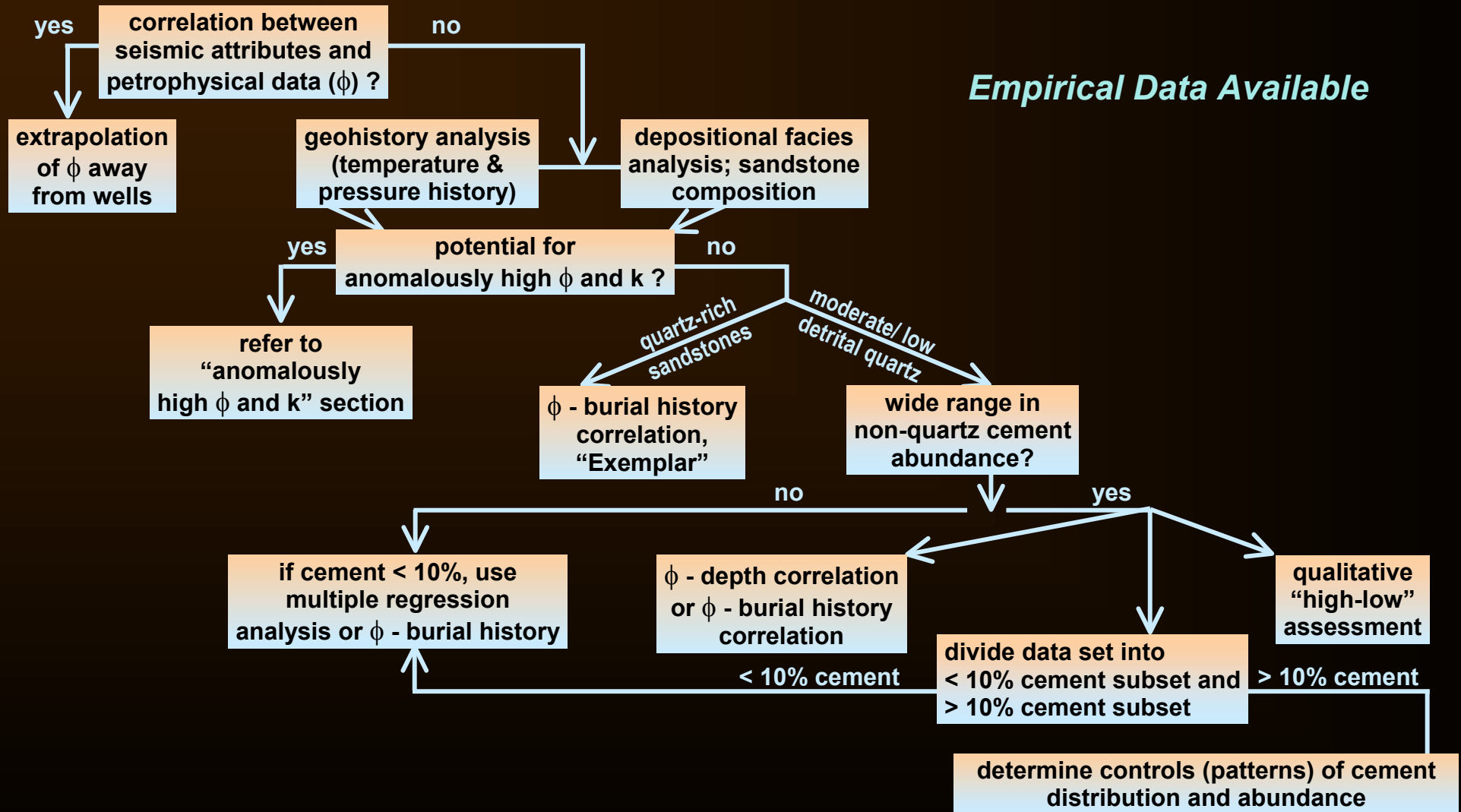
# Approaches to Reservoir Quality “Prediction”



# Requirements for Adequate Predictions

- ▶ **High predictive accuracy should be achieved from a limited number of geological input parameters**
- ▶ **Input parameters should be simple enough to be estimated from available geological information with reasonable confidence**
- ▶ **Prediction should be based on multiple techniques**

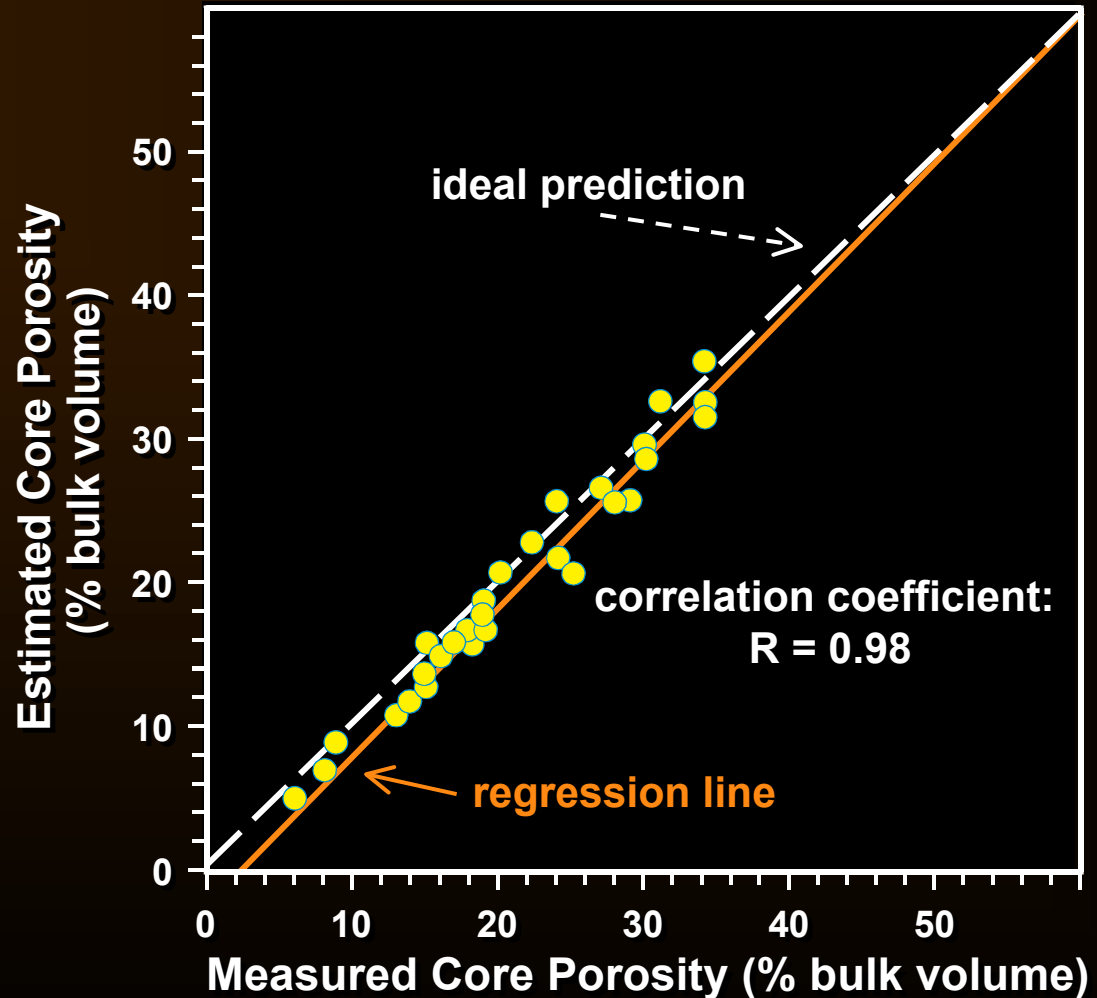
# Pre-Drill Prediction/Assessment of Porosity and Permeability in Mature Basins



(modified from Bloch and Helmold, 1995)

# “Global” Porosity Prediction Equation for sandstones with < 5% cement

$$\phi = 18.60 + (4.73 \times \ln \text{quartz}) + (17.37/\text{sorting}) - (3.8 \times \text{depth} \times 10^{-3}) - (4.65 \times \ln \text{age})$$

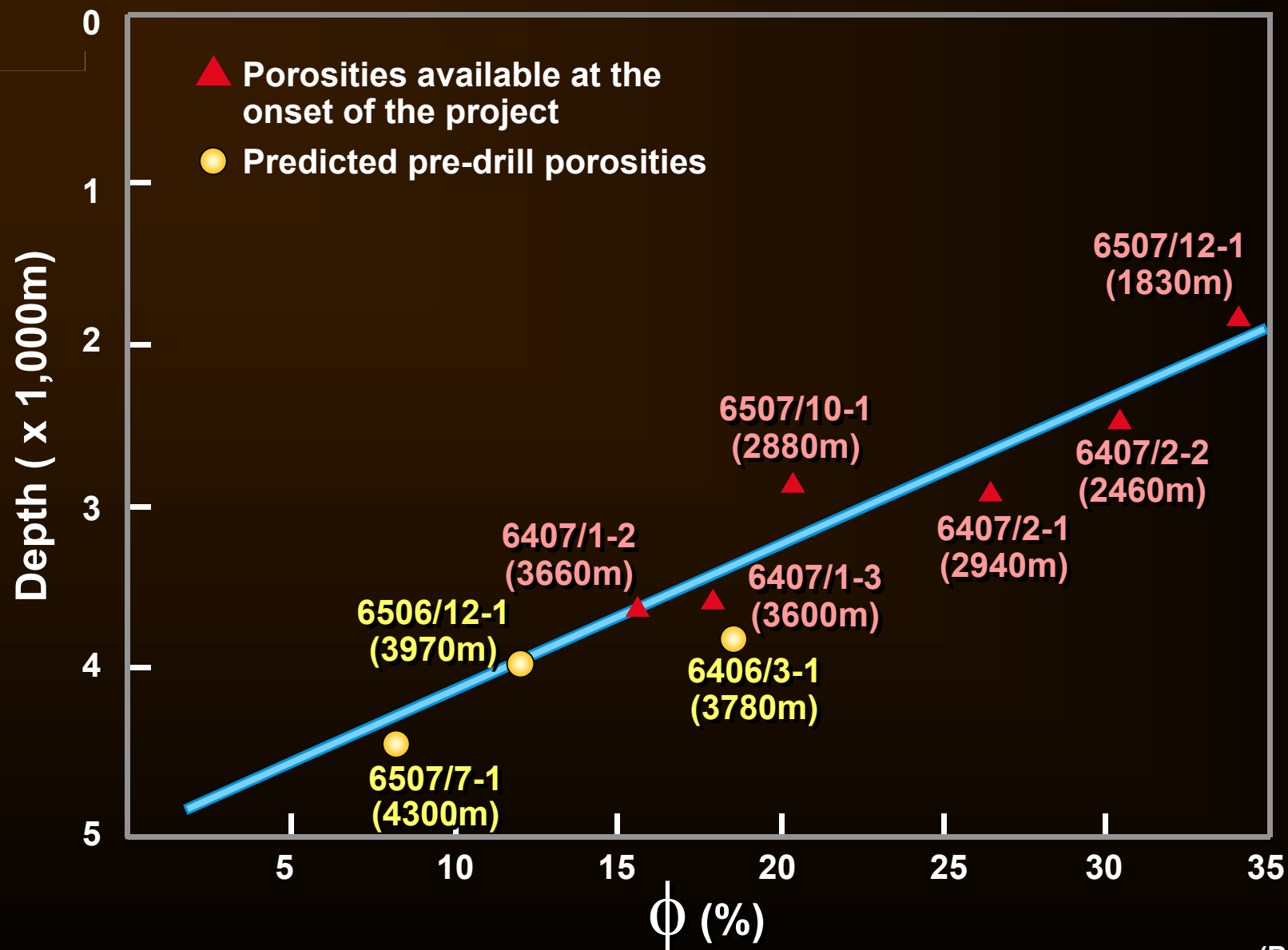


(Scherer, 1987)

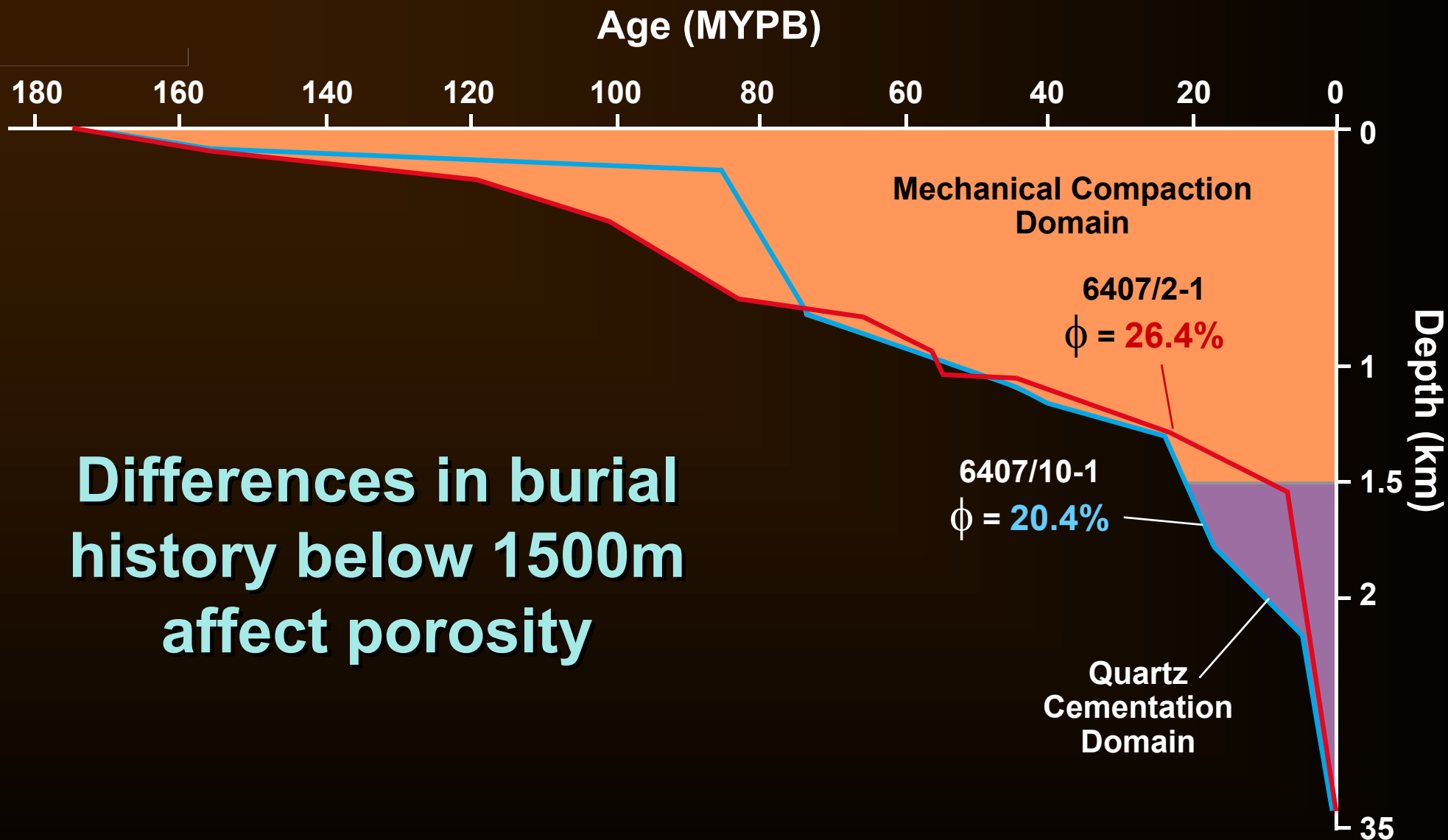
# Approximate Ranges in Cement Volumes for Different Styles of Diagenesis

Style of Diagenesis	Range in Volume of Principal Cement	Range in Volume of Ancillary Cements
Quartz dominated	5 -15% (increases with temperature of burial)	3 - 5%, <5% late carbonate*
Clay dominated	10 - 20% (only illite dominated increases with temperature of burial)	< 5% quartz, <5% late carbonate*
Early clay/late quartz	5 - 10% clay, < 5% quartz	< 5% late carbonate*
Early carbonate/ evaporite dominated	≤ 20 - 30% (increases in proximity to evaporites/saline lake deposits)	
Zeolite	5 - 20% (increases with increasing lithic content)	≤ 10% clay, ≤ 10% late carbonate*

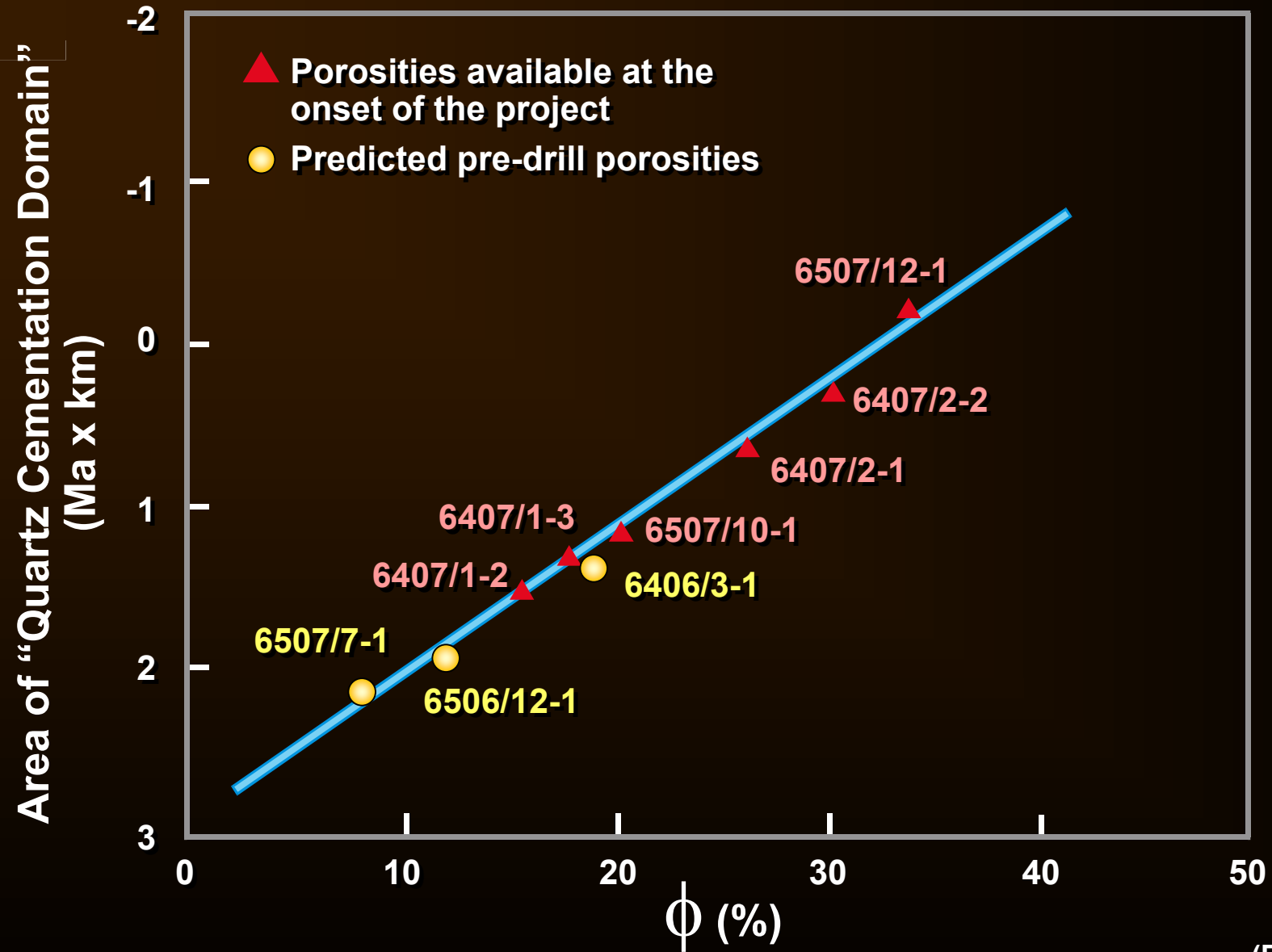
\*Can be locally < 20 - 30%



(Bloch, 1994)

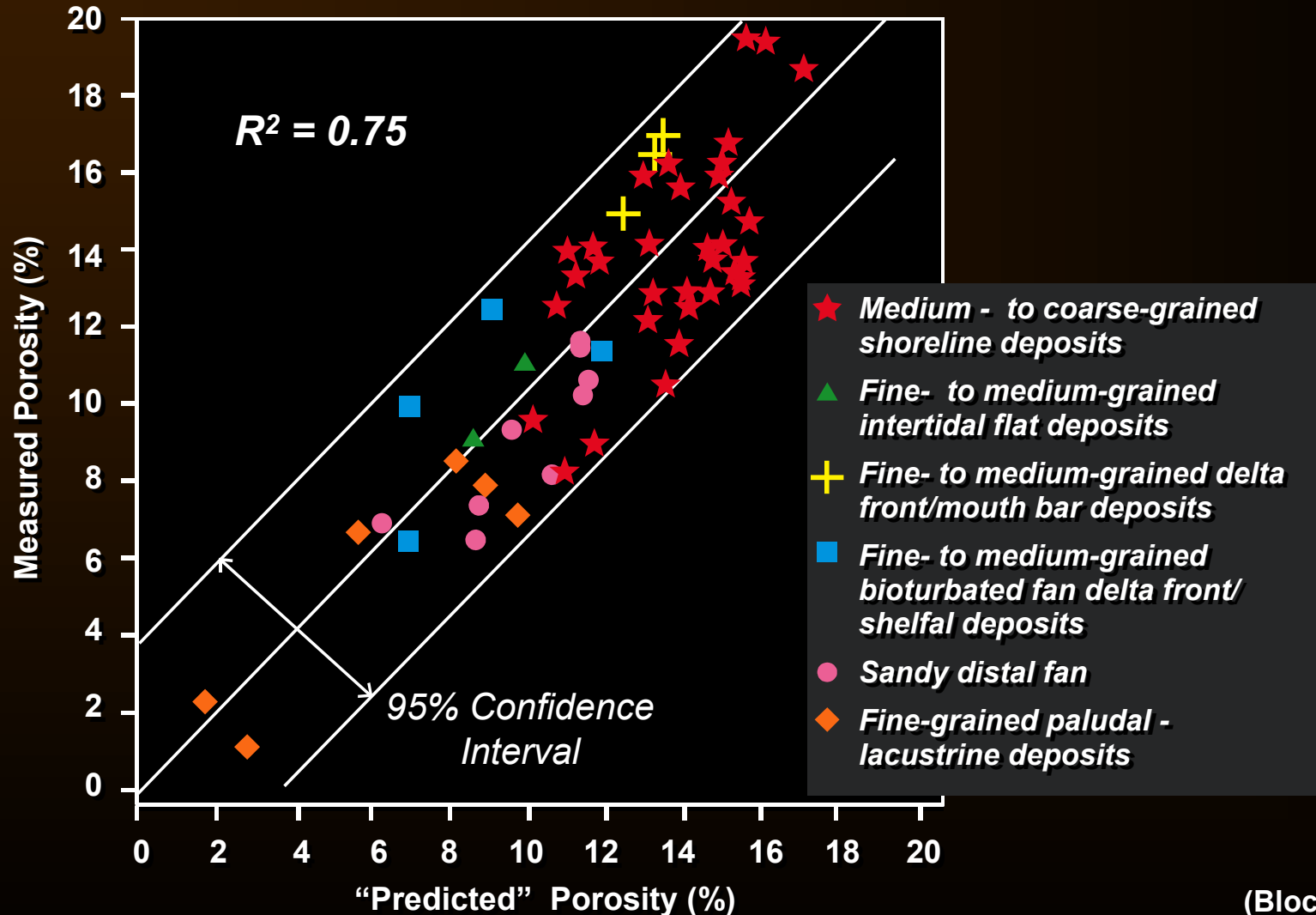






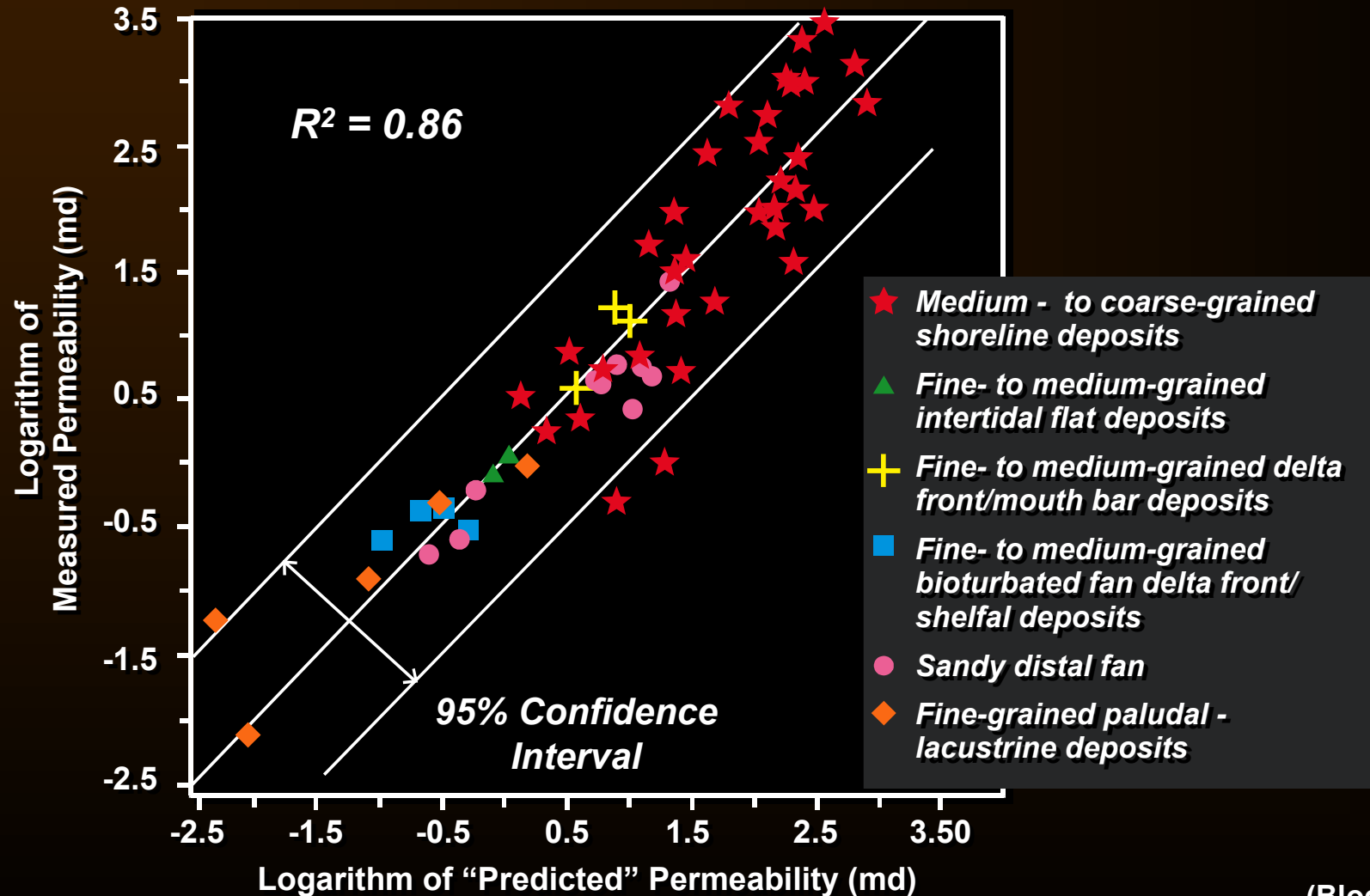
(Bloch, 1994)

$$\text{Porosity (\%)} = -6.1 + 9.8 (1/\text{sort}) + 0.17 (\text{Rigid Grain Content})$$



(Bloch, 1994)

$$\text{Log}_{10} (\text{PERM}) = - 4.67 + 1.34 (\text{grsz}) + 4.08 (1/\text{sort}) + 3.42 (\text{R}/100)$$



(Bloch, 1994)

# Example of a Porosity & Permeability Prediction in Sandstones: Summary

## Input Data

- A. Outcrop samples and samples from closest wells
- B. “Best estimate” burial/thermal history data

## Porosity Prediction Approaches

### Approach 1

- 1. Use “best estimate” thermal history data to calculate present-day vitrinite reflectance values in target (based on Burnham & Sweeney kinetic model)
- 2. Use Schmoker & Hester regression equations of  $R_o$  vs. porosity

### Approach 2

- 1. Use “Exemplar” to simulate mean porosity and cement abundance evolution
- 2. Calculate permeability
- 3. Use Monte Carlo analysis to obtain probabilistic porosity predictions

<u>Predicted Total Mean Porosity</u>			
		$R_o$ - Porosity regression	“Exemplar”
Po. ss	10 <sup>th</sup> percentile	7%	9%
Po. ss	50 <sup>th</sup> percentile	11%	14%
Po. ss	90 <sup>th</sup> percentile	15%	19%
Mu. ss	10 <sup>th</sup> percentile	13%	13%
Mu.ss	50 <sup>th</sup> percentile	18%	19%
Mu.ss	90 <sup>th</sup> percentile	23%	24%

# Example of a Porosity & Permeability Prediction in Sandstones: Input

## A. Expected Lithology in the Proposed Well

(Based on upthrust outcrop samples and samples from closest wells)

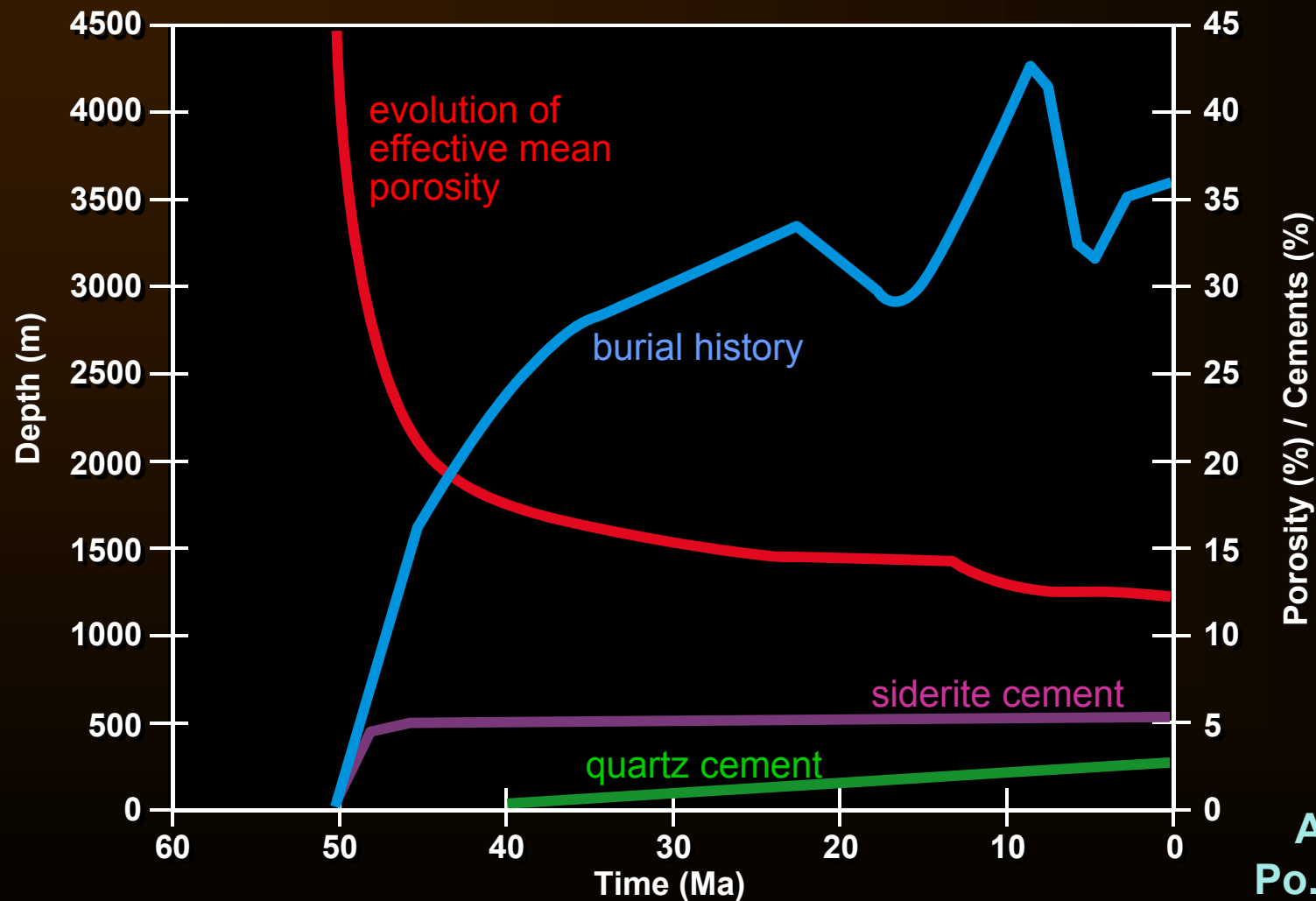
1. Detrital composition: quartz-rich (> 85% quartz)
2. Texture: medium to coarse grain size (~0.50mm), moderate sorting

## B. Diagenesis

*Diagenetic History:*

Siderite	very early (<40° C)	
Kaolinite		Compaction
Quartz	>75°	
Fracturing	(fractured quartz)	
Ankerite	(minor ankerite in fractures)	
Oil Emplacement	(oil in fractures)	
Uplift	oxidation of siderite and precipitation of hematite	

# Predicted Evolution of Effective Porosity and Cement Abundances



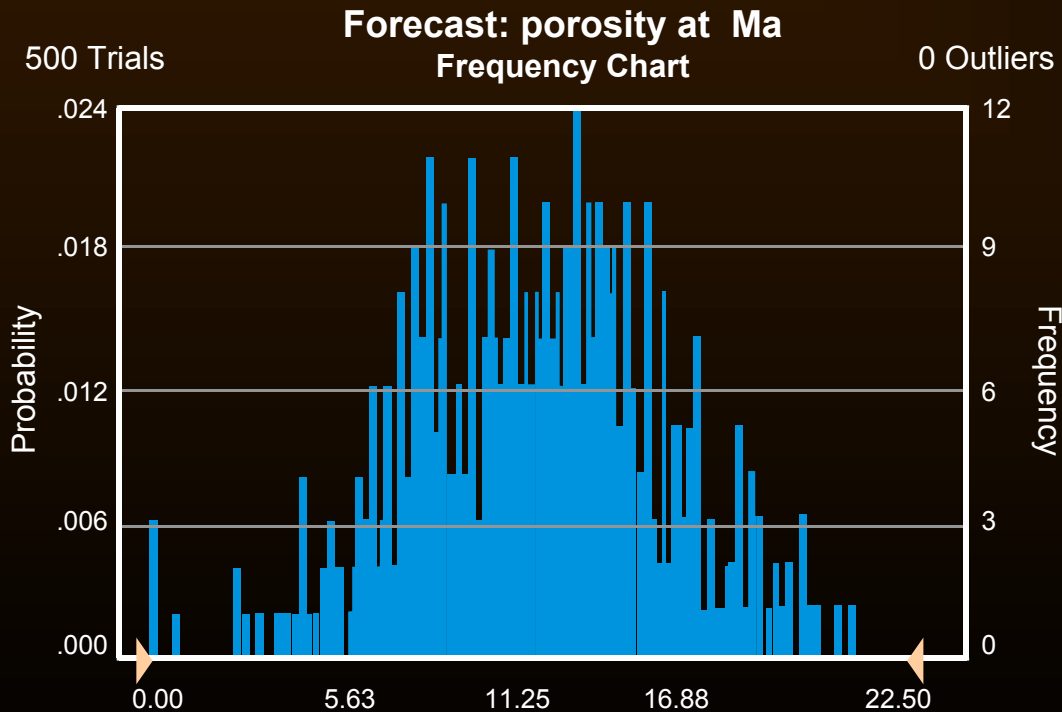
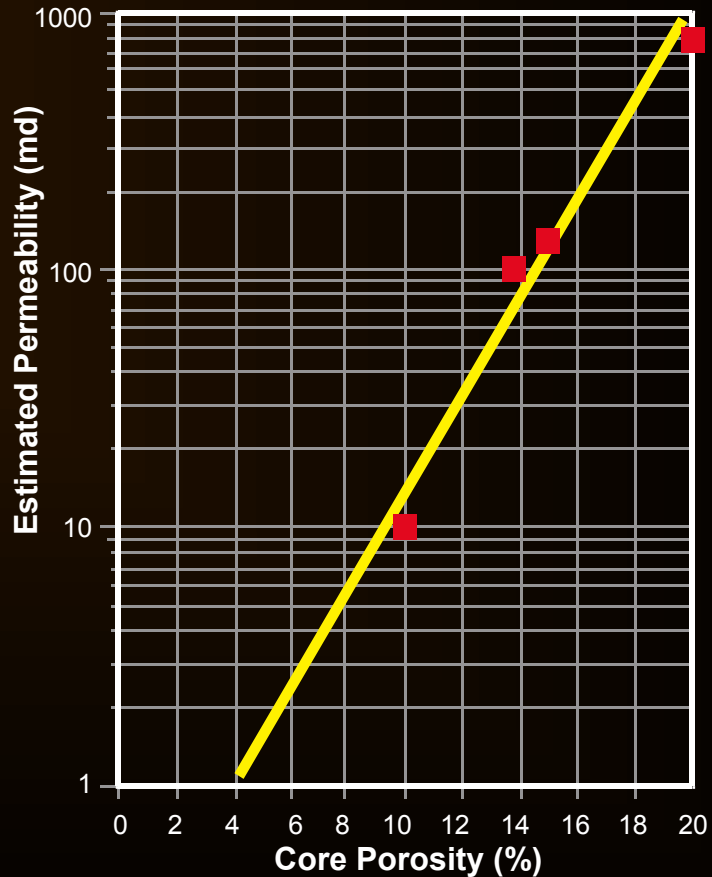
AG-1 Well,  
Po. Sandstone

Forecast: porosity of Po. Fm. At 0 Ma

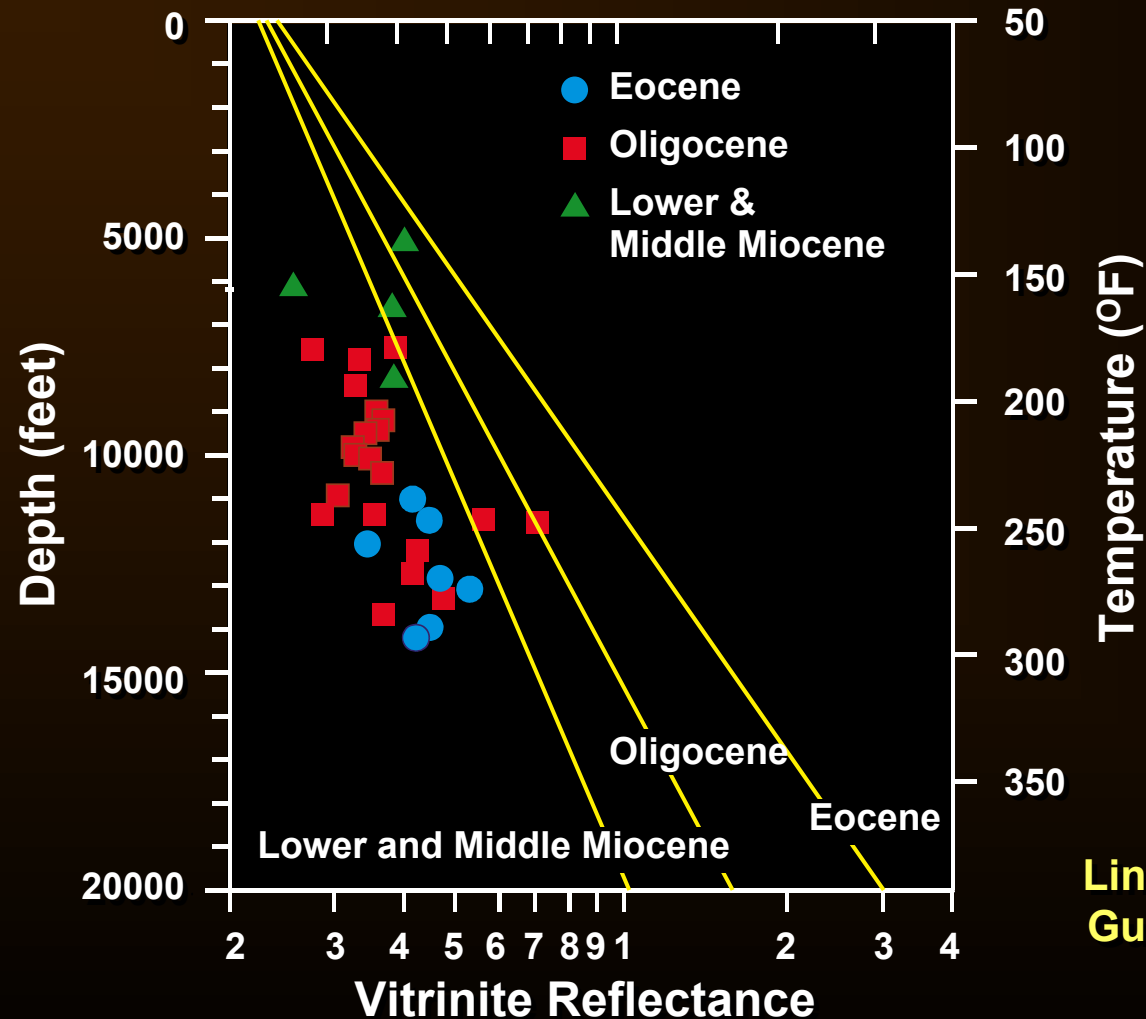
		% Effective Porosity
P10	10%	6.75
	20%	8.14
	30%	9.25
	40%	10.31
P50	50%	11.35
	60%	12.24
	70%	13.06
	80%	14.06
P90	90%	15.65

## Example of a Porosity & Permeability Prediction in Sandstones: Output

Permeability = f (effective porosity, average grain size of 0.50mm, <10% clay)



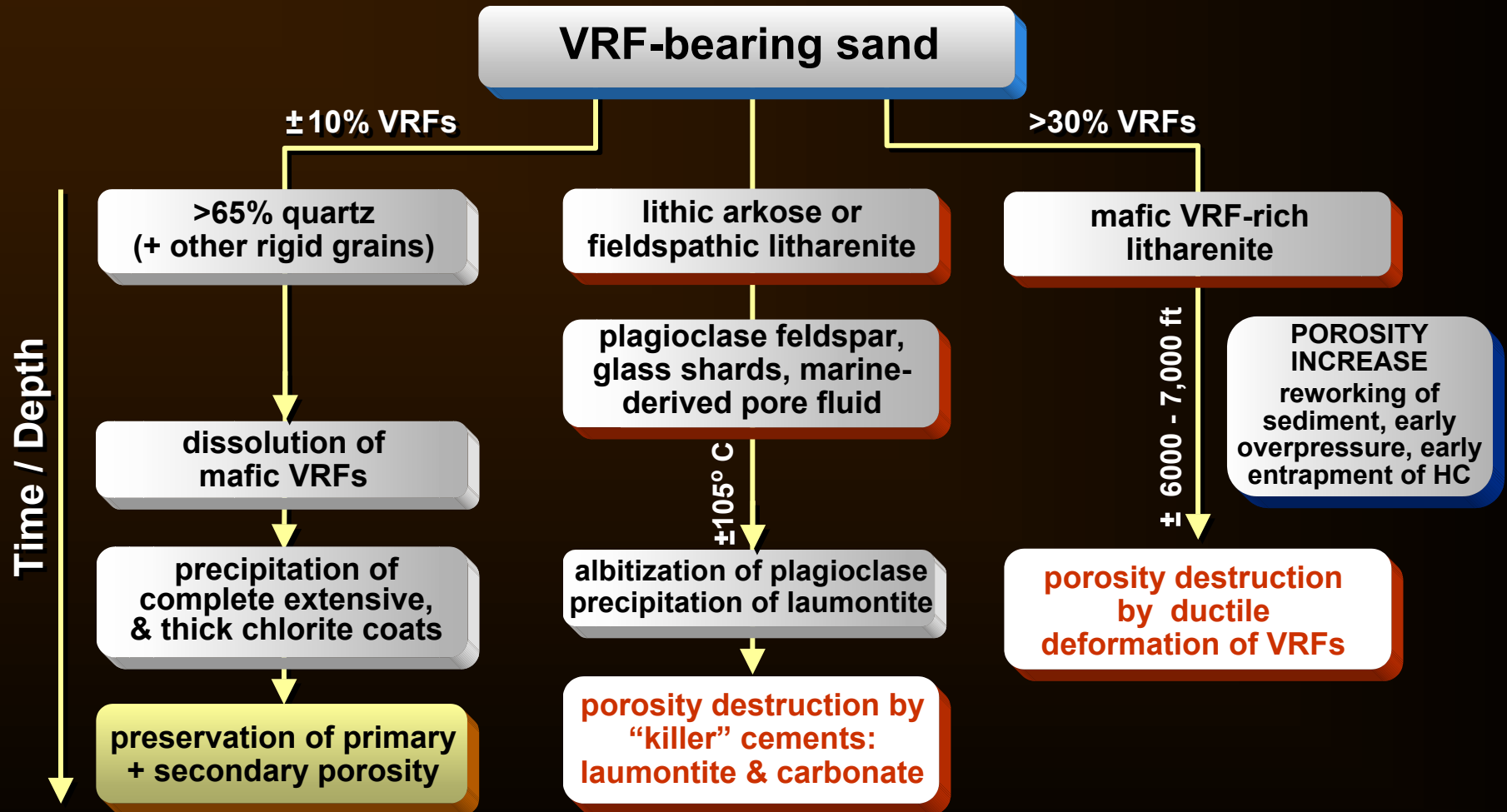
# VR values in the southern San Joaquin basin do not correlate with depth of burial



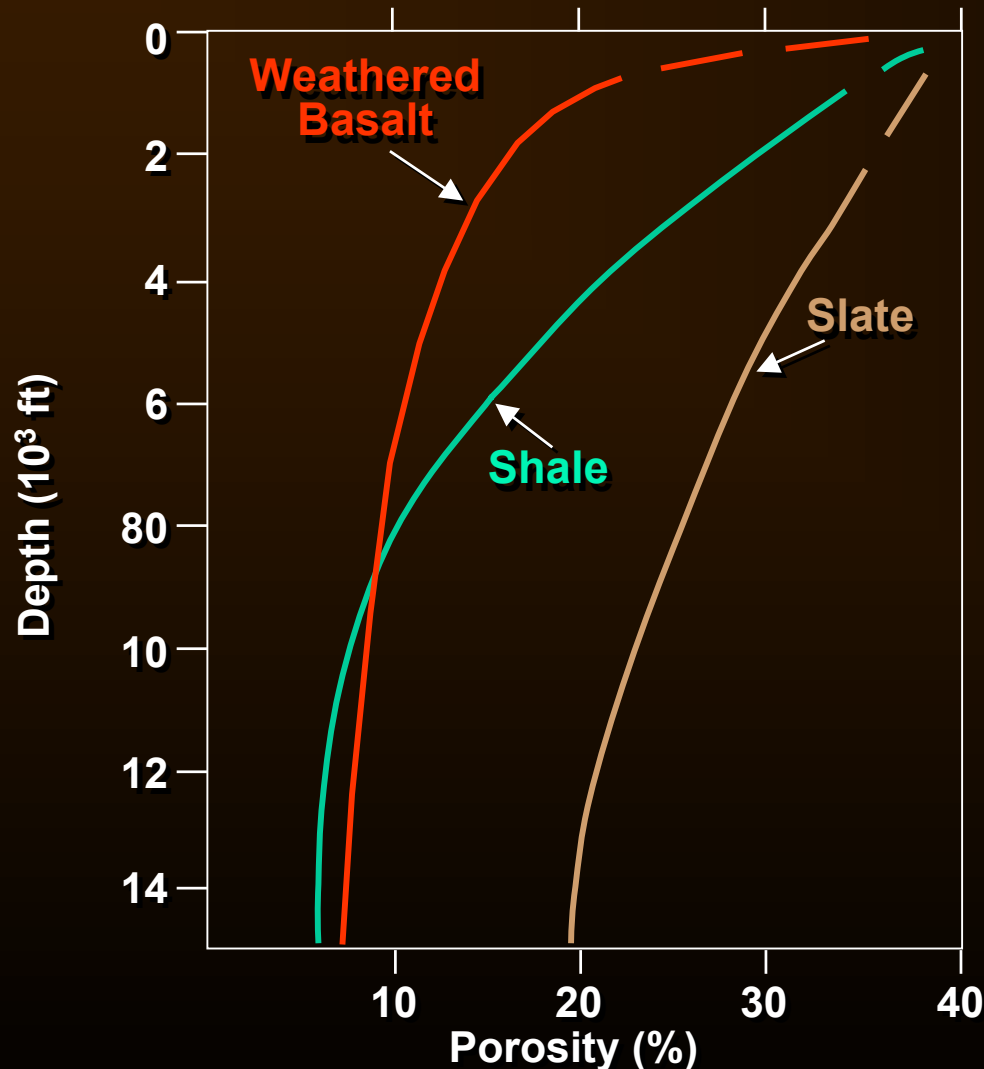
Lines denote trends for  
Gulf Coast sandstones  
(from Dow, 1978)



# Reservoir Quality in Volcaniclastic Sandstones



# Compaction Model with 50% Quartz: 50% Lithic Sands for Slate, Shale and Weathered Basalt



## Effect on Curve

### Decreases Porosity

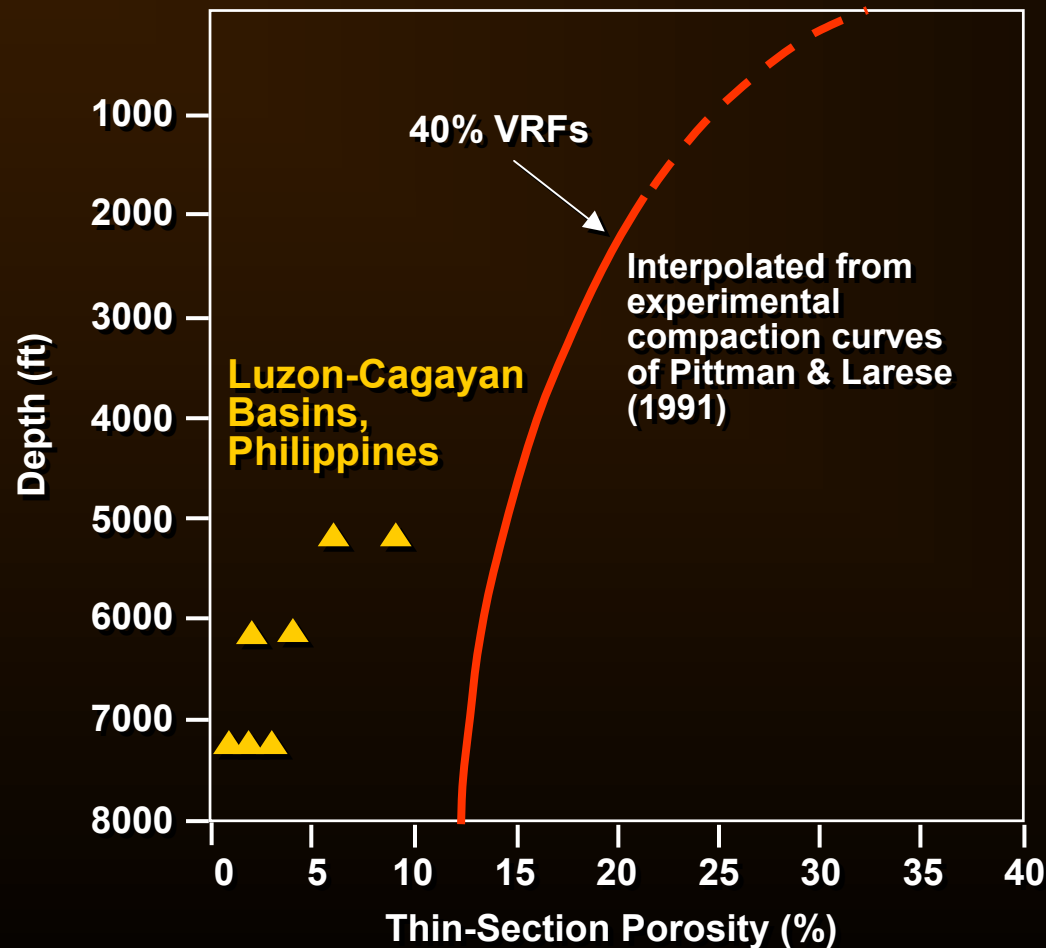
- High geothermal gradient
- Decrease in sorting
- Cement (Depends on Timing)

### Increases Porosity

- Relatively early overpressure
- Creation of secondary porosity
- Entrapment of hydrocarbons

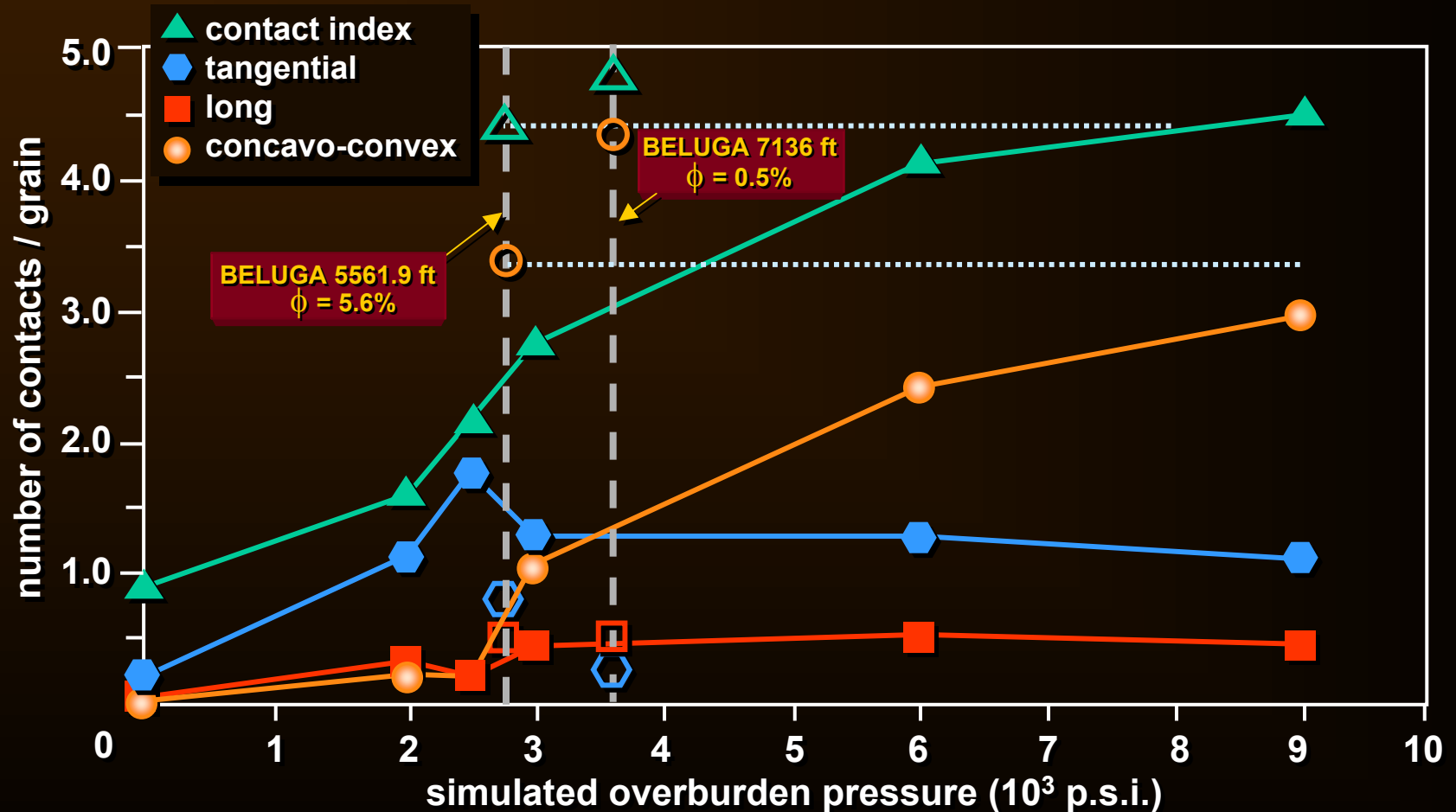
(from Pittman & Larese, 1991)

**In moderately-sorted, VRF-rich (>35% VRFs) sandstones, reservoir quality is drastically reduced below approximately 6,000 ft**



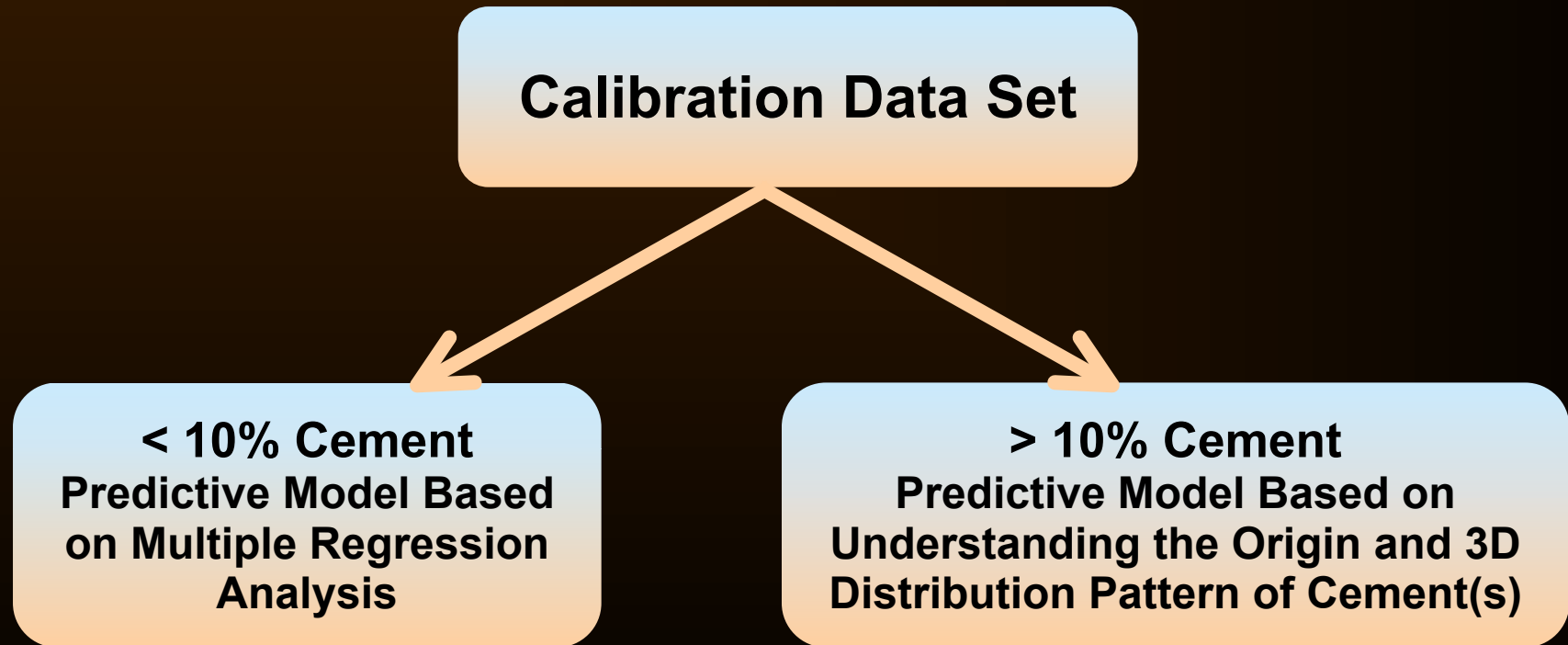
# Comparison of Geologic & Experimental Compaction

Contact index and contact types as a function of simulated overburden pressure, for compaction tests conducted with Eagle River sand and triaxial overburden apparatus



(from Kurkcy, 1988)

# Approach to Reservoir Quality Prediction in Sandstones with a Wide Range of Pore-Filling Cements



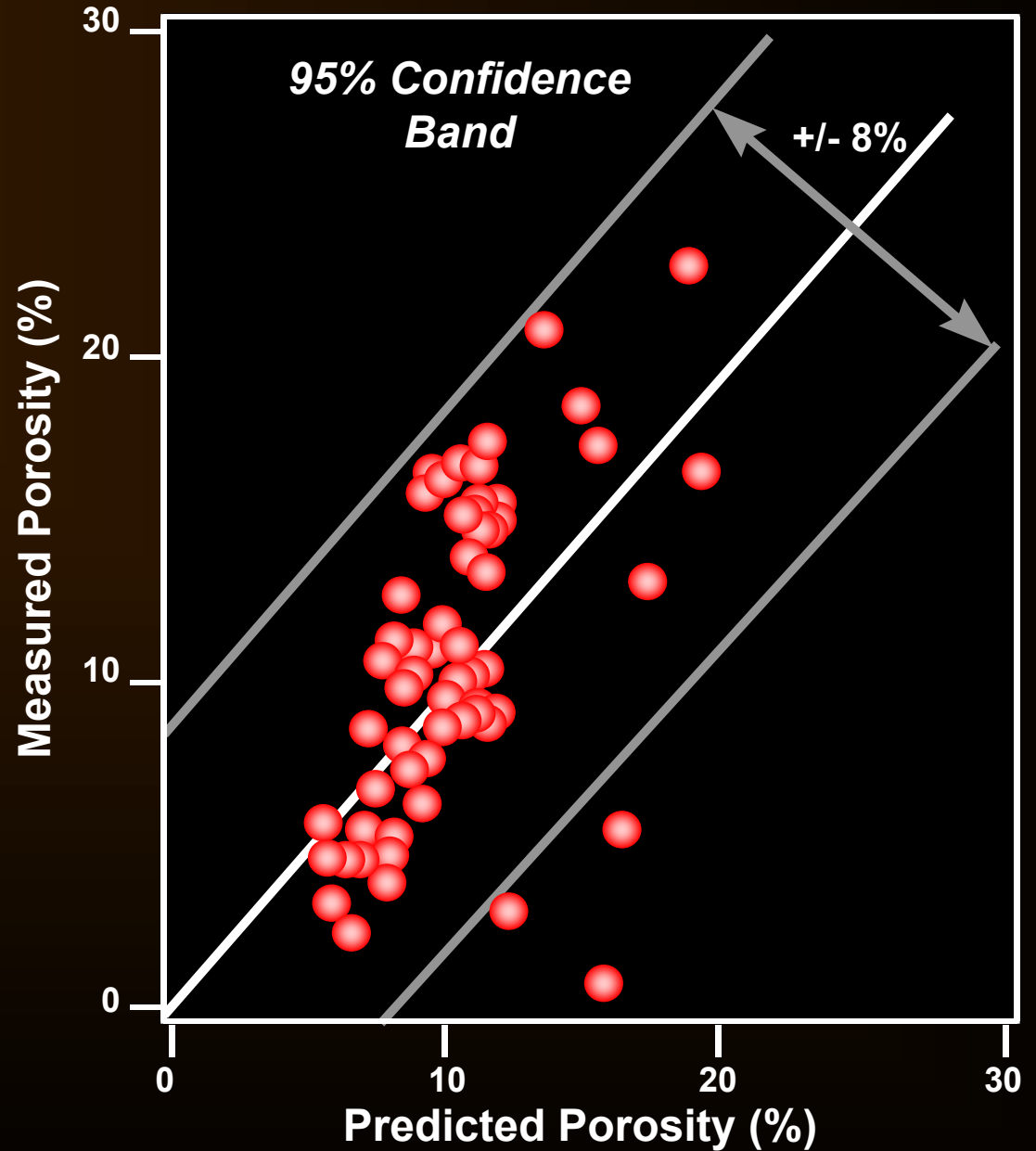
# Conclusions

**Occurrence and Abundance of Laumontite** in Middle Eocene-Late Oligocene Arkosic Sandstones of the San Emigdio Area Exhibit Distinct Patterns:

<b>Temperature</b>	<b>&gt;215° F (~100° C)</b>
<b>Geologic Time</b>	<b>Most Abundant in Upper Oligocene</b>
<b>Areal Distribution</b>	<b>South of the White Wolf Fault; Abundance Decreases Systematically from N to S (Increasing Distance from Volcanic Center ?)</b>

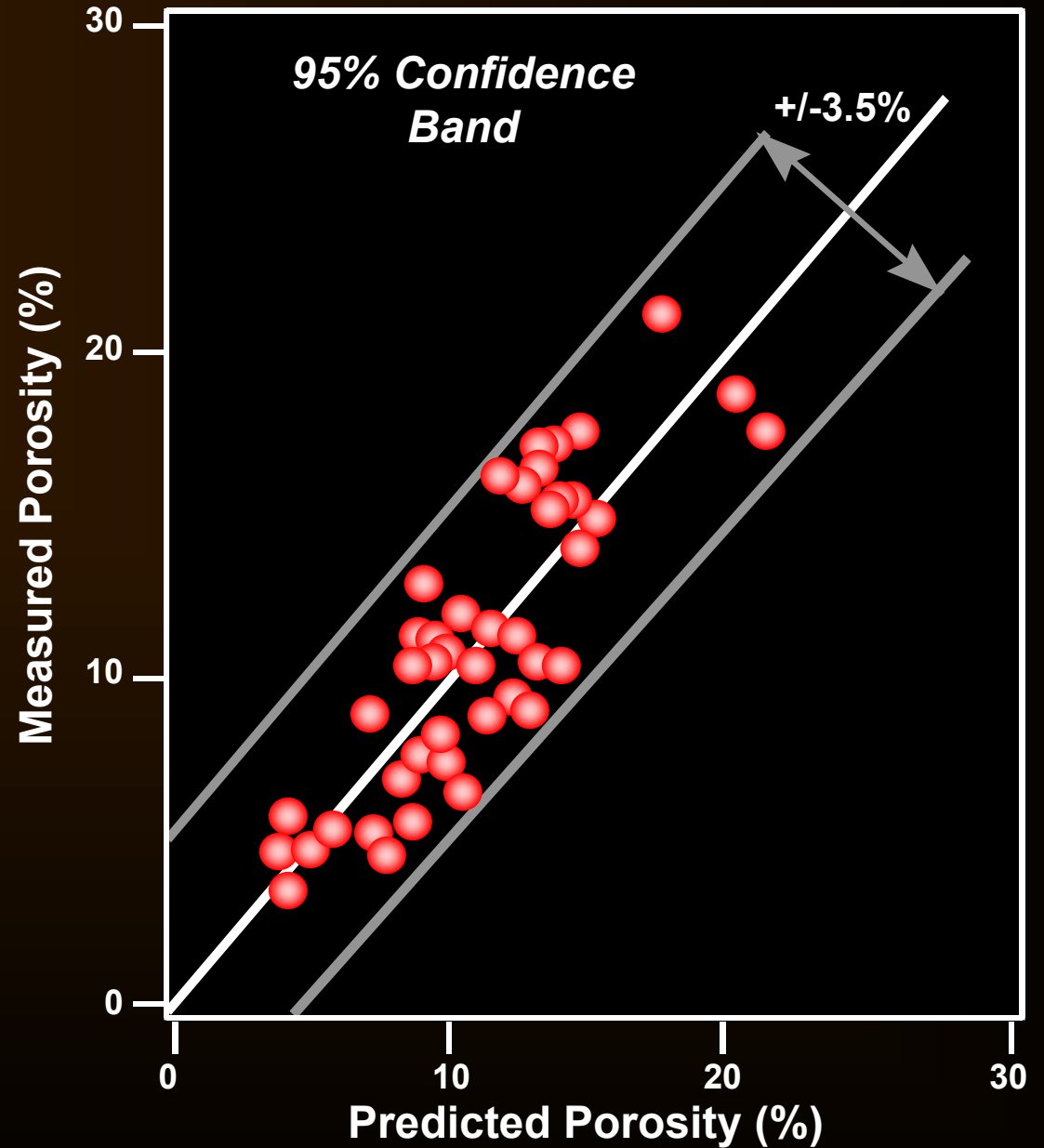
# Measured vs Predicted Porosity

Regression on Detrital Matrix  
and Depth for All Samples



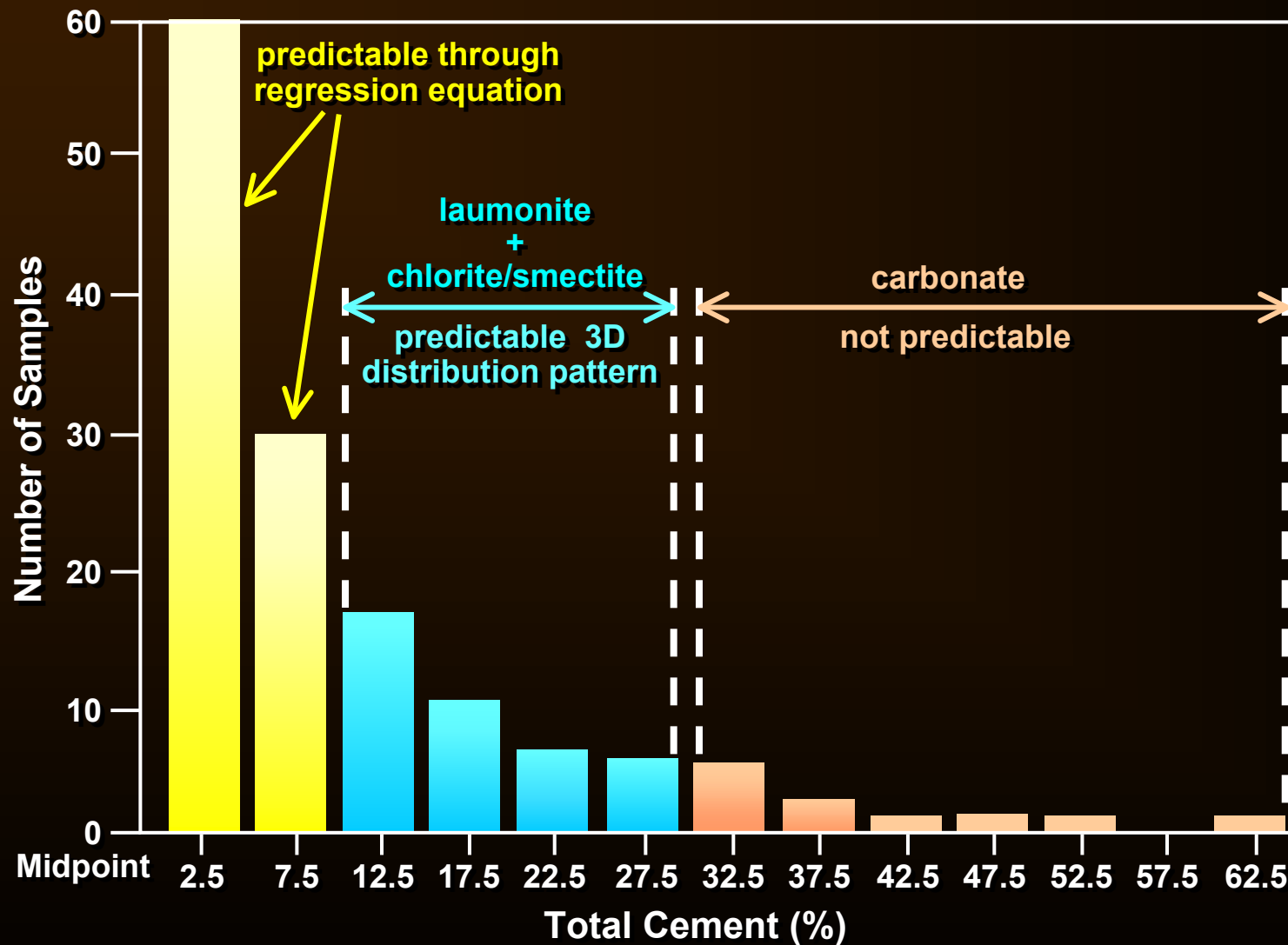
# Measured vs Predicted Porosity

Regression on Detrital Matrix  
and Depth for Samples  
with <10% Cement

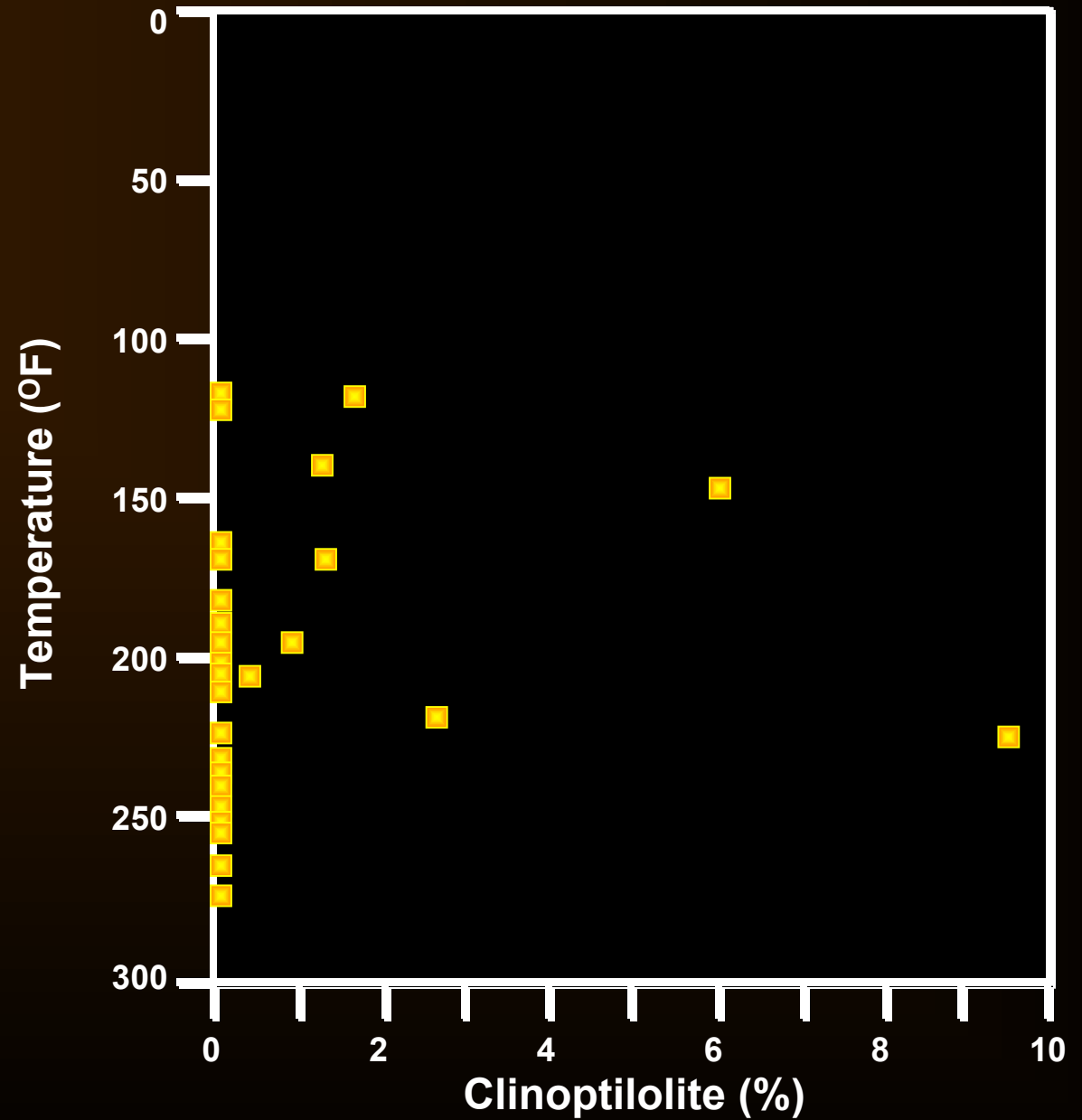




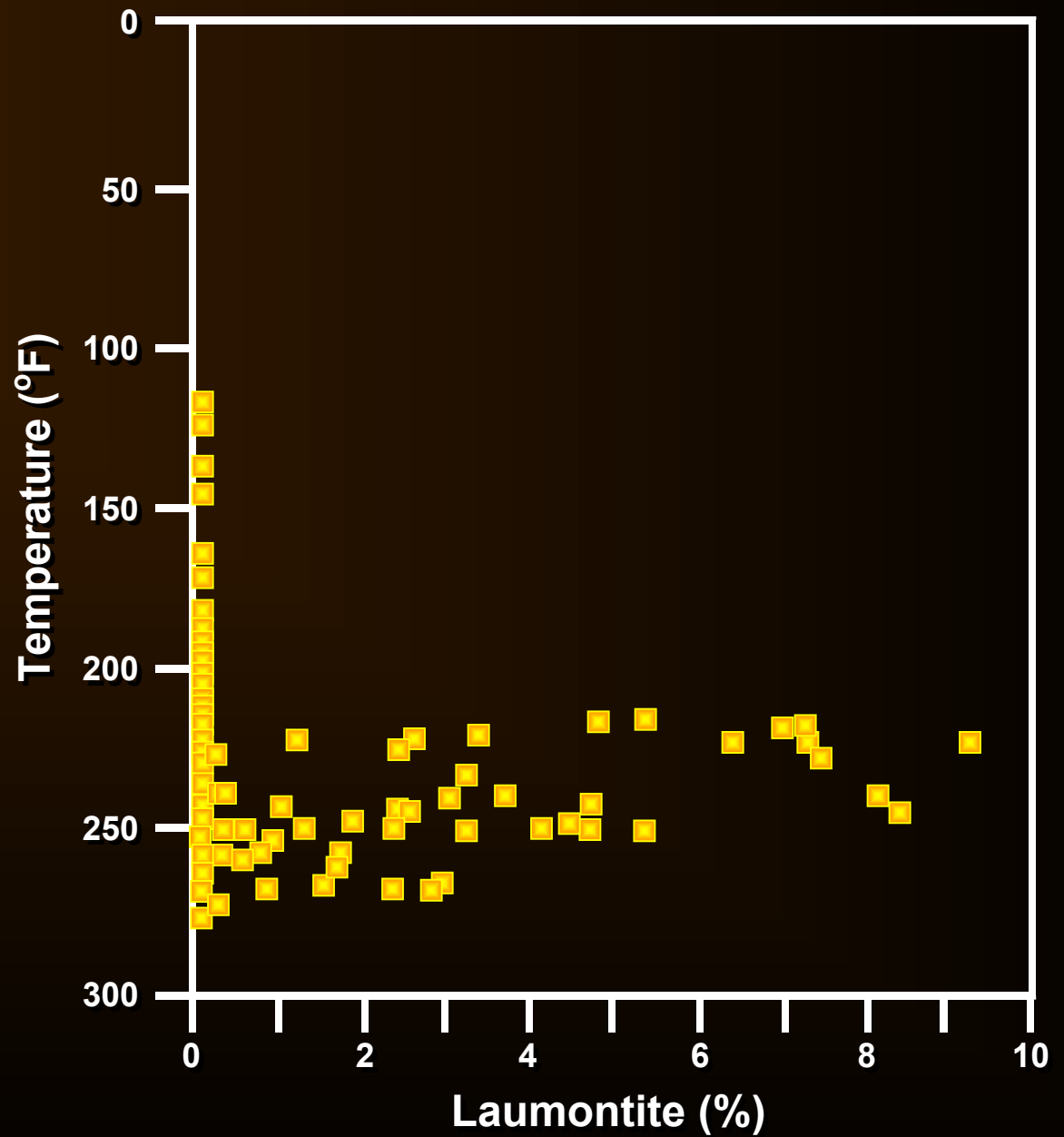
# Three Prediction Subsets



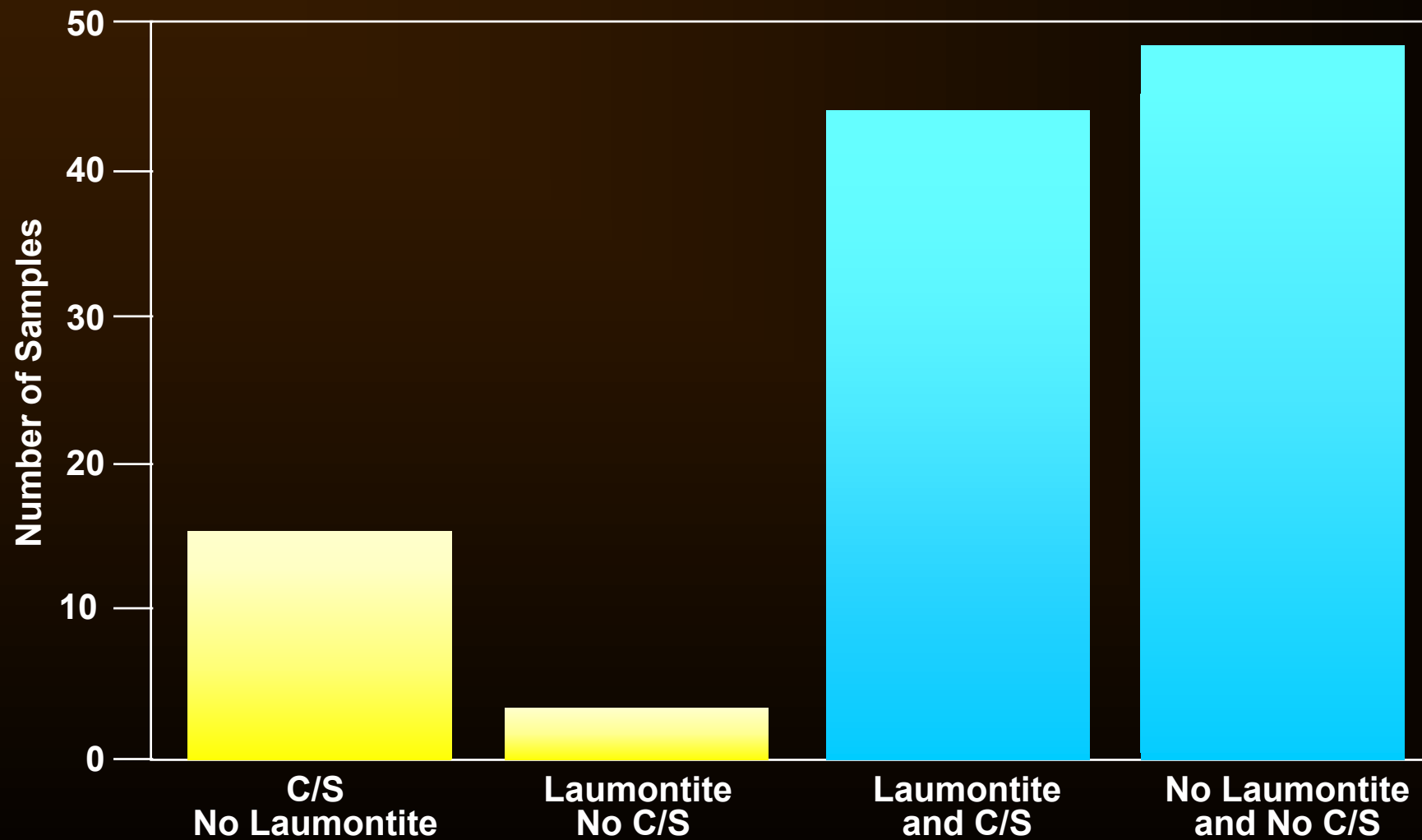
**Clinoptilolite  
Occurs  
Only Below  
215° F**



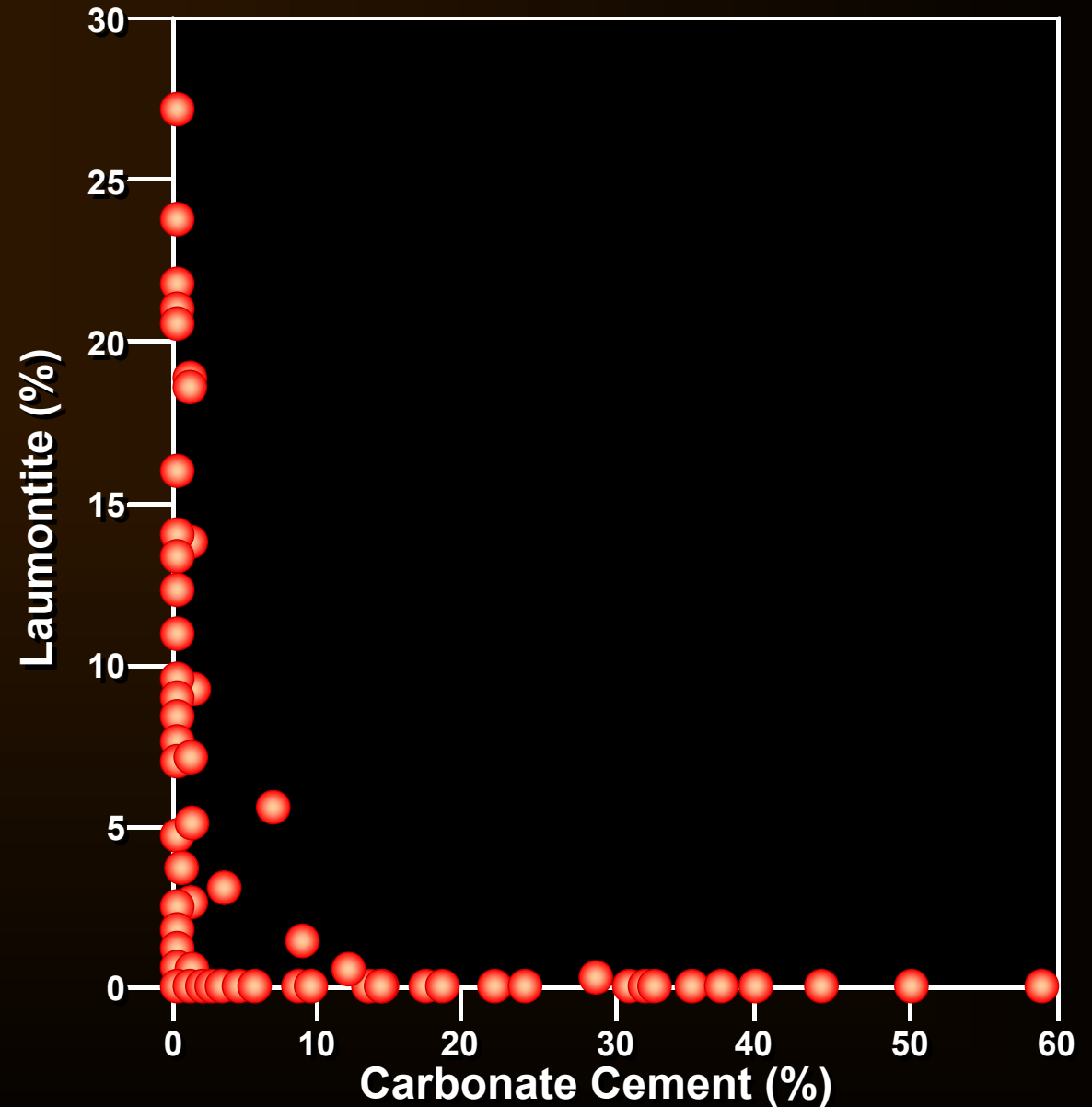
**Laumontite  
Occurs  
Only Above  
215° F**



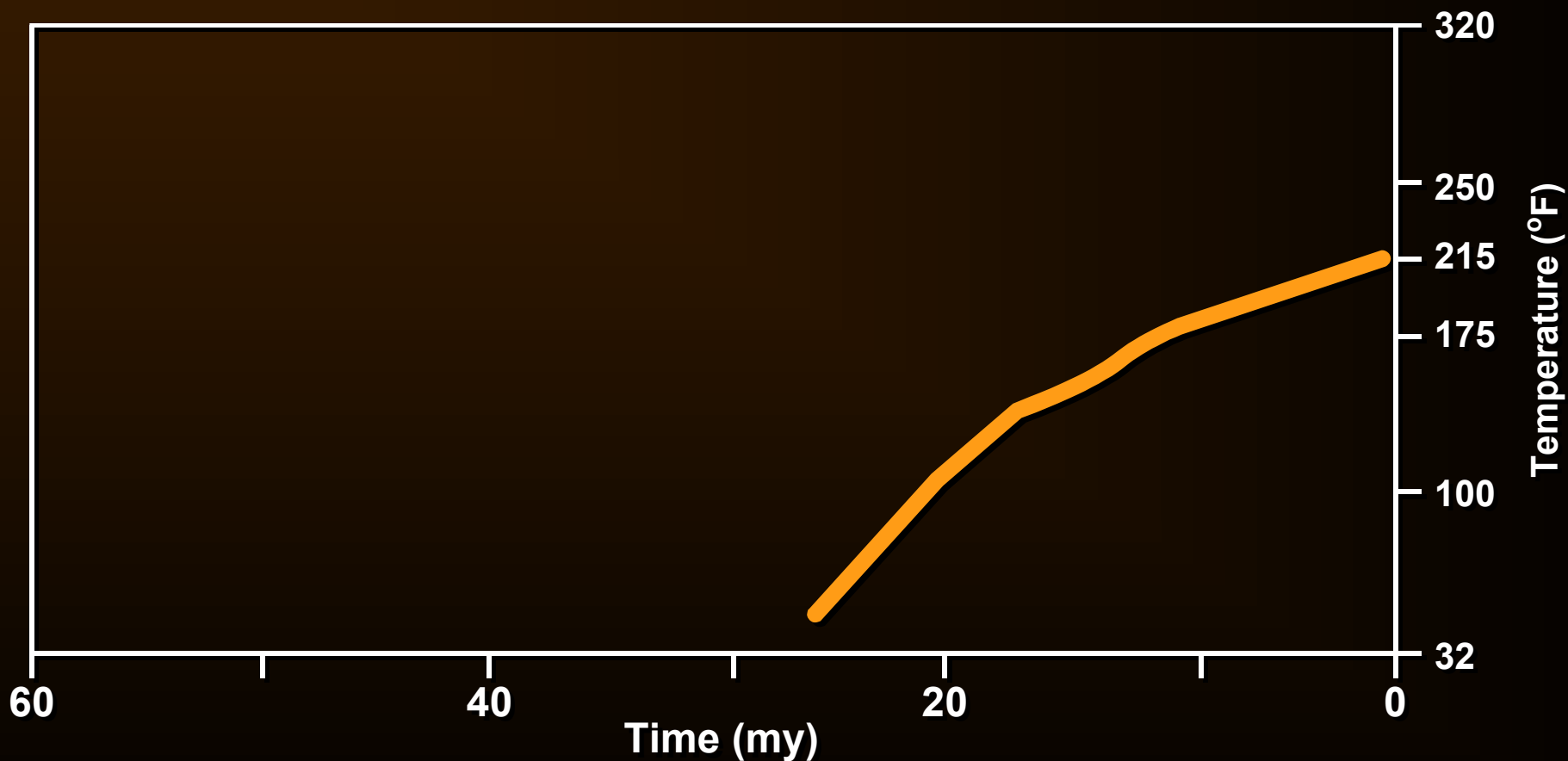
# Chlorite/Smectite and Laumontite Display a Sympathetic Relationship on a Thin-Section Scale



# Laumontite and Carbonate Cements Are Mutually Exclusive



# Some of the Laumontite is Geologically Very Young



**At Temperatures > 225° F, Zeolite Abundance in Zemorrian ss (late early & late Oligocene) Decreases from North to South (?)**

